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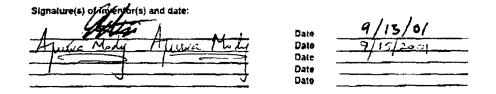
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 ANTAL 5.04

Efficient Training and Synchronization Sequence Structures for MIMO OFDM

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Abstract— In this invention we present a general method of forming efficient sequence structures which can be used for parameter estimation as well as synchronization. As a specific example we fabricate a structure using directly modulatable orthogonal polyphase sequences. We presente a technique by which the transmission matrices for each subcarrier is made unitary hence satisfying the MMSE criterion for channel estimation. A search was then carried out for structures with lowest peak to average power ratios. For systems employing 2 transmit antennas, Alamouti's structure and the simplified orthogonal structure are found to be optimal. The simplified structure obtained from orthogonal design is also optimal for systems employing 4 and 8 transmit antennas. For systems employing 3 transmit antennas, circulant structure is the most suitable.

I.INTRODUCTION

Orthogonal Frequency Division Multiplexing (OFDM) has become popular for wireless communications [1]. A multicarrier system can be efficiently implemented in discrete time using Inverse Discrete Fourier Transform (IDFT) to act as a modulator. The actual data to be transmitted, now reperesent "frequency" domain coefficients of the signal and the samples at the output of the IDFT stage are in the "time" domain.

In this paper we present efficient training and synchronization sequence structures for Multi Input Multi Output (MIMO) OFDM systems. For OFDM systems synchronization must be carried out both in time and frequency. In addition, OFDM systems require parameter estimation of the channel and the noise variance. Parameter estimation is normally carried out using a suitable training sequence. An efficient sequence structure must be suitable for synchronization as well as parameter estimation. Additionally for OFDM systems the

The authors wish to thank the Yamacraw initiative, of the State of Georgia, U. S. A. <u>http://www.yamacraw.org</u> for supporting this research.

synchronization signal must have a low Peak to Average Power Ratio (PAPR).

In the IEEE 802.11a Standard [1] synchronization and training sequence consists of a short sequence followed by a long sequence. The short sequence is used for time synchronization and coarse frequency offset estimation whereas the long sequnce is used for fine frequency offset and channel estimation. This sequence is not designed for use in MIMO OFDM systems.

In this paper we will be using the words "training" and "synchronization" sequence interchangeably since we propose an efficient sequence structure that can be used for both synchronization as well as training. We propose to use directly modulatable orthogonal polyphase sequences to form the MIMO synchronization sequence. The sequence structure is modified such that it is also suitable for MIMO parameter estimation.

II.ANALYSIS

A block of N samples at the output of the OFDM modulator represents an OFDM symbol and the net time required to transmit one symbol is called the symbol time, T_s . Later, a cyclic prefix consisting of the last G samples of the output of the IDFT block are inserted in front of the OFDM symbol samples. The time length of the cyclic prefix should be greater than the maximum length of the channel impulse response. The main function of the cyclic prefix is to guard the OFDM symbol against Inter Symbol Interference (ISI), hence, this cyclic prefix is called the guard interval of the OFDM symbol and has a time duration T_q . The samples are then applied to a pair of balanced D/A converters, and the analog I and Q signals are later upconverted to RF. The OFDM signal is transmitted over the channel, received and downconverted to base band. The guard interval is removed from the received discretized downconverted signal and the signal is demodulated using a Discrete Fourier Transform (DFT) on a block of N sam-

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ples. In this paper, samples in the frequency domain are represented by *Capital* alphabet and those in the time domain are expressed using *small* alphabet.

The general transmission format for a $Q \times L$ spacetime system is shown in Fig. 1. Such a space-time system consists of Q Antennas at the transmitter and LAntennas at the receiver separated from each other in such a manner that the received signals have a minimum correlation. A system employing such a scheme can provide a diversity of the order of $Q \times L$. Let

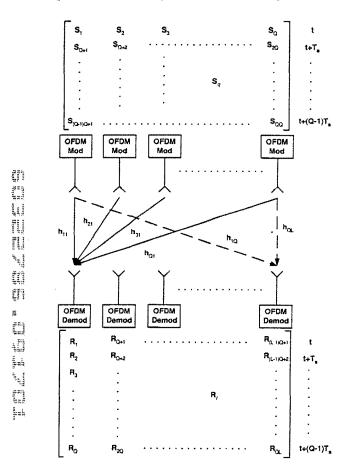


Fig. 1. Block diagram of a system with $Q \times L$ transmitreceive diversity

 \underline{S}_q =(transmitted OFDM symbol), $\underline{\eta}_{ij}$ = (vector of channel coefficients in the frequency domain between the *i*th transmit and the *j*th receive antenna) and \underline{R}_l =(the received demodulated OFDM symbol). Pilots in the form of known OFDM symbols are sent for at least Q symbol periods (QT_s) in order to obtain a unique solution for the channel coefficient estimates. If the pilots are sent for more than Q symbol periods then we would obtain a Least Squares (LS) solution at an expense of a larger overhead. The OFDM symbol period is given by $T_s = NT + T_g$ where 1/T is the sample rate into the OFDM modulator (bit rate for BPSK modulation).

The time period T_g corresponds to the transmission of G samples. Often it is a good practice to double the length of the guard time in the training period [1]. This helps in synchronization, frequency offset estimation and equalization for channel shortening in case that the length of the channel exceeds the length of the guard time. An IDFT/ DFT pair is used as the OFDM modulator/ demodulator. The N point IDFT output sequence for the qth OFDM symbol is given by

$$s_{q,n} = \frac{1}{\sqrt{N}} \sum_{k=0}^{N-1} S_{q,k} \exp\left\{j\frac{2\pi nk}{N}\right\} \quad 0 \le n \le N - 1$$
(1)

where $\{S_{q,k}\}_{k=0}^{N-1}$ is the transmitted data sequence from the *i*th transmit Antenna such that q = (i-1)Q + cwhere $1 \leq c \leq Q$. The signal is then sent over the channel. The notation for the received signals vectors for the time instants $(t, t+T_s, ..., t+(Q-1)T_s)$ are $(\underline{r}_1, \underline{r}_2, ..., \underline{r}_Q)^T$, ..., $(\underline{r}_{Q\cdot(l-1)+1}, \underline{r}_{Q\cdot(l-1)+2}, ..., \underline{r}_{Q\cdot l})^T$,..., $(\underline{r}_{(L-1)\cdot Q+1}, \underline{r}_{(L-1)\cdot Q+2}, ..., \underline{r}_{QL})^T$ for the Antennas 1, 2, ..., L. The received sample sequence after the removal of the guard interval for the (vT_s) th training slot is

$$r_{l,n} = \sum_{i=1}^{Q} \sum_{m=0}^{M-1} h_{ij,m,v(N+G)+n} s_{i,(n-m)N} + w_{l,n} \quad (2)$$

where $h_{ij,m,v(N+G)+n}$ is the channel impulse response at lag *m* and instant v(N+G) + n and *l* can be expressed as l = (j-1)Q + d for $1 \le d \le Q$. The $w_{l,n}$ are complex additive white Gaussian noise samples with variance N_0 . The received sample sequence $\{r_{l,n}\}_{n=0}^{N-1}$ is demodulated as [2]

$$R_{l,k} = \mathrm{DFT}\{r_l\}(k) \tag{3}$$

$$= \sum_{i=1}^{Q} S_{i,k} \eta_{ij,k} + W_{l,k}.$$
 (4)

Hence the received demodulated OFDM sample matrix \mathbf{R}_k of dimension $(Q \times L)$ for the kth subcarrier can be expressed in terms of the transmitted sample matrix \mathbf{S}_k of dimension $(Q \times Q)$, the channel coefficient matrix η_k of dimension $(Q \times L)$ and the additive white Gaussian noise matrix \mathbf{W}_k of dimension $(Q \times L)$ as

$$\mathbf{R}_{k,Q \times L} = \mathbf{S}_{k,Q \times Q} \cdot \boldsymbol{\eta}_{k,Q \times L} + \mathbf{W}_{k,Q \times L}$$
(5)

R, η and **W** can either be seen as N, $Q \times L$ dimensional matrices or as $Q \times L$ length-N vectors.

The total energy emenated from the Q transmit antennas is restricted to unity [2] such that,

$$\mathbf{E}\left\{\sum_{q=1}^{Q}|s_{q,n}|^{2}\right\} = 1 \qquad n = 0, 1, 2, ..., N.$$
(6)

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