

Pathloss-Aided Closed Loop Transmit Power Control for 3G UTRA TDD

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Abstract – In 3G UTRA TDD, closed loop power control is used as an inner loop power control technique for downlink DPCHs (dedicated physical channels) in the 3.84 Mcps option, and both uplink and downlink DPCHs in the 1.28 Mcps option. In the current closed loop power control, transmit power is generally updated at the frame/sub-frame rate, using a semi-static step size (1, 2, or 3 dB). Such a slow transmit power update by a given step size may not be enough to cope with dynamically changing environments, so that the performance of the closed loop power control is degraded. In this paper, we propose an enhanced closed loop power control technique for UTRA TDD, which adapts the step size according to relative pathloss (or power) measurements at the transmitter side. We show that the link-level performance of the proposed power control can be significantly better than the existing closed loop power control. The largest gains are obtained for slow and moderate fading channels.

I. INTRODUCTION

3G UTRA TDD (Third Generation UMTS Terrestrial Radio Access Time Division Duplex) uses a hybrid time division and code division multiple access scheme. In TDD, multiple user communications are sent over a shared frequency spectrum in both uplink and downlink. As specified in the 3GPP specifications [1], UTRA TDD consists of two options: 3.84 Mcps option and 1.28 Mcps option. For DPCHs (Dedicated Physical Channels) in both options, quality based transmit power control is used as a link adaptation method, such that it adjusts the transmit power of the DPCHs in order to achieve a desired quality of service with minimum transmit power, thus limiting the interference level in the system. The transmit power control can be divided into two processes operating in parallel: inner loop power control and outer loop power control. The inner loop is to keep the received SIR (Signal-to-Interference Ratio) of DPCHs as close as possible to a target SIR value. The outer loop sets the target SIR for the inner loop, based on quality estimates like BLER (Block Error Rate) of the transport channel(s) associated with the DPCHs. In [10], an outer loop algorithm is discussed. Here we focus on the inner loop power control. One scheme to implement the inner loop power control is an SIR-based closed loop power control applied to downlink DPCHs for the 3.84 Mcps option and both uplink and downlink DPCHs for the 1.28 Mcps option. The current TDD closed loop power control typically operates at a

frequency of 100 Hz and 200 Hz in the 3.84 Mcps option and 1.28 Mcps option, respectively. When channel conditions are highly dynamic, the closed loop power control with the rather slow power control update rate for the UTRA TDD may not be able to cope with the dynamic channel conditions fast enough. As a result, the performance of the closed loop power control will be degraded. Accordingly it is highly desirable to develop a power control algorithm being capable of fast adapting to channel conditions. In [2], it was shown that the performance of downlink closed loop power control could be improved by signaling the difference between measured SIR and target SIR.

In this paper we present an enhanced closed inner loop power control technique for the UTRA TDD, called "Pathloss-aided closed loop transmit power control". It exploits the UTRA TDD characteristics: channel reciprocity between uplink and downlink and usage of a training sequence at a fixed transmit power level within specific timeslots like P-CCPCH (Primary-Common Control Physical Channel) [3]. Multi-path propagation conditions are discussed based on the 3GPP standard [7]. In addition, link-level simulations are carried out over the various multi-path fading conditions, in order to evaluate the current closed loop power control and proposed scheme.

II. UTRA TDD INNER LOOP POWER CONTROL

The inner loop power control schemes for DPCHs in UTRA TDD fall into two categories: open loop power control and closed loop power control.

A. Open loop power control

Open loop power control uses the received power measurement of a reference channel which is transmitted on a regular basis with known transmit power. In 3.84 Mcps TDD, uplink dedicated physical channels are dynamically power controlled by open loop control [4]. P-CCPCH (or other beacon channels) is used for the pathloss measurement. In addition to the pathloss estimate, the UE uses power-control related parameters to determine the transmit power required to achieve the target quality. The parameters are signaled by the UTRAN and include the uplink interference, the target SIR from the outer loop, a weighting factor, and a constant value.

Due to the channel reciprocity between downlink and uplink in UTRA TDD, the open loop control is capable of tracking propagation channel variations. In particular when the delay between the power-controlled transmission and the pathloss measurement is small, the open loop control can quickly compensate for fading channels. The drawback of the open loop control is that it is affected by errors in the absolute power level measurement and power setting [5]. The errors are caused mainly due to the non linear RF amplifier in the transmitter and receiver. However some of the errors can be compensated by using an outer loop power control [6].

B. Closed loop power control

Closed loop power control makes use of feedback information, called "TPC command", signaled from the receiving station of the communication link. The closed loop is employed for downlink dedicated physical channels in 3.84 Mcps TDD and both uplink and downlink dedicated physical channels in 1.28 Mcps TDD. In both TDD options, the receiving station generates TPC commands indicating either "power up" or "power down" according to comparison between SIR measurement of dedicated channels and a target SIR value. At the transmitting station, depending on the received TPC command, the transmit power of dedicated physical channels is adjusted by a pre-defined step size taking the value of 1, 2, 3 dB. For a given closed loop power controlled link, the step size is a CCTrCH (Coded Composite Transport Channel) specific parameter and semi-static.

In UTRA TDD, the closed loop power control is performed on a CCTrCH basis such that the individual TPC command is paired with at least one power controlled CCTrCH. Pairing of TPC command(s) and power controlled CCTrCH(s) is determined by the RNC (Radio Network Controller) and signaled to the UE and NodeB. In general, the closed loop power update rates per CCTrCH in 3.84 Mcps TDD and 1.28 Mcps TDD are 100 Hz and 200 Hz, respectively, which are slow compared to 1500 Hz in UTRA FDD. Furthermore, in the case that either the power controlled link transmission or the TPC command carrying link transmission is paused, the closed loop power control operates at a further slower rate.

Due to the use of a fixed step size and the slow update rate for the closed loop power control in UTRA TDD, a short-term dynamic range of the transmission power step would be limited. Table 1 shows the maximum transmission power step range after receiving 5 TPC commands, which is given by the standard [7]. Here a TPC command group is a set of TPC command values derived from a corresponding sequence of TPC commands of the same duration.

Table 1. Closed loop power control range in UTRA TDD

Step size	Transmitter power control range after 5 equal TPC command groups	
	"Up"	"Down"
1 dB	+4 <= P <= +6	-6 <= P <= -4
2 dB	+8 <= P <= +12	-12 <= P <= -8
3 dB	+12 <= P <= +18	-18 <= P <= -12

III. MODELING OF PROPAGATION CONDITIONS

It is assumed that for the performance analysis of UTRA TDD power control schemes we consider propagation conditions for multi-path fading environments such that the average power level of each propagation channel case is equal to zero in dB. The rationale for this assumption is that the inner loop power control schemes used for UTRA TDD (FDD as well) can fairly well overcome slow fading propagation conditions [8]. In particular we focus here on the multi-path propagation conditions specified in the 3GPP standard [7]. Note that the performance requirements in the standard are specified under multi-path fading conditions. Table 2 shows examples of such propagation conditions. All taps have classical Doppler spectrum. Figure 1 shows channel power patterns for the Case 1 channel and ITU Vehicular A channel (VA 30) with 30km/h, respectively. It is observed that the channel power can considerably fluctuate by 20 – 30 dB, depending on the propagation condition.

In addition, Table 3 presents the statistics of channel power difference in dB between consecutive 10 msec spaced intervals. It should be noted that in 3.84 Mcps TDD the closed loop power control update occurs every 10 msec (per frame) in a normal operation mode. We see that the statistics of the channel power difference are different with different channel conditions. This indicates that the current TDD closed loop power control using a fixed step size can be enhanced by adapting step size according to channel variations.

Table 2. Examples of propagation conditions for multi-path fading environments

Case 1 Speed 3km/h		Case 2 Speed 3 km/h	
Relative Delay [ns]	Relative Mean Power [dB]	Relative Delay [ns]	Relative Mean Power [dB]
0	0	0	0
976	-10	976	0
		12000	0
ITU Pedestrian A Speed 3km/h (PA3)		ITU Vehicular A Speed 30km/h (VA30)	
0	0	0	0
110	-9.7	310	-1.0
190	-19.2	710	-9.0
410	-22.8	1090	-10.0
		1730	-15.0
		2510	-20.0

Table 3. Statistics of channel power difference between consecutive 10 msec spaced intervals

Propagation condition	Mean (dB)	Variance (dB)
Case 1	1.5	1.3
Case 2	0.6	0.3
Case 3	3.2	4.0
VA 30	2.2	2.1

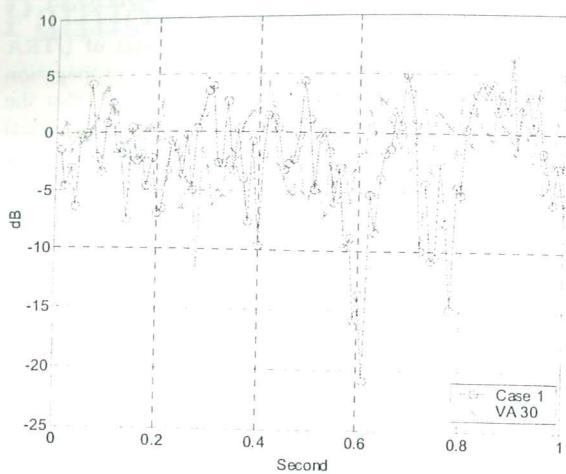


Figure 1. Power in dB of multi-path fading channels

IV. PATHLOSS AIDED CLOSED LOOP POWER CONTROL

In this section, we propose an enhanced closed loop power control scheme for UTRA TDD, which enables the transmitter to autonomously vary the step size in accordance to channel variations. By using the downlink/uplink channel reciprocity in UTRA TDD, relative pathloss measurements are used by the transmitter to estimate the variations. The proposed scheme can be described as follows:

$$P(k) = P(k-1) + \Delta_{TPC}(b_{TPC}(k), \Delta PL(k)) \quad (1)$$

where $P(k)$ is the transmit power level in dBm at the k^{th} power update. $\Delta_{TPC}(b_{TPC}(k), \Delta PL(k))$ represents the power control step size in dB as a joint function of two variables, $b_{TPC}(k)$ and $\Delta PL(k)$, denoting the transmit power control (TPC) command and relative pathloss estimate, respectively, for the k^{th} power update. For simplicity of notation let us use $b_{TPC}(k)=1$ for "power up" and $b_{TPC}(k)=-1$ for "power down". The relative pathloss estimate, $\Delta PL(k)$, is determined by

$$\Delta PL(k) = (\alpha L(k) + (1-\alpha)L_0(k)) - (\alpha L(k-1) + (1-\alpha)L_0(k-1)) \quad (2)$$

where $L(k)$ is the most recent available pathloss estimate in dB before the k^{th} power update. It is assumed that the pathloss measurement is based on a reference channel with known transmit power, for example, P-CCPCH (or other beacon channels) used in UTRA TDD. Here the pathloss measurement is implemented by subtracting in dB the received measured P-CCPCH power from the reference P-CCPCH transmit power. $L_0(k)$ is the long-term average pathloss in dB. $0 \leq \alpha \leq 1$ is a weighting factor, which may be determined according to radio channel condition and the delay, expressed in timeslots, between the reference P-CCPCH timeslot and the power controlled timeslot(s). It should be

noted that although absolute pathloss measurement generally suffers from a systematic measurement error, the error can be eliminated when relative pathloss measurements are used.

Figure 2 provides a flowchart of step size determination in the transmitter. This is an example of a possible implementation of Equation (1). As a response to the received TPC command, the transmitter does either increase or decrease its transmit power level, as in the current closed loop power control. However the step size for the power adjustment with the proposed scheme is varied based on the relative pathloss estimate. In case where the channel varies in a direction opposite to the corresponding TPC command such that $b_{TPC}(k)=1$ and $\Delta PL(k)<0$ or $b_{TPC}(k)=-1$ and $\Delta PL(k)>0$, the transmit power is adjusted by a minimum step size, Δ_{Min} . For the sake of simplicity, integer-valued step sizes are considered here.

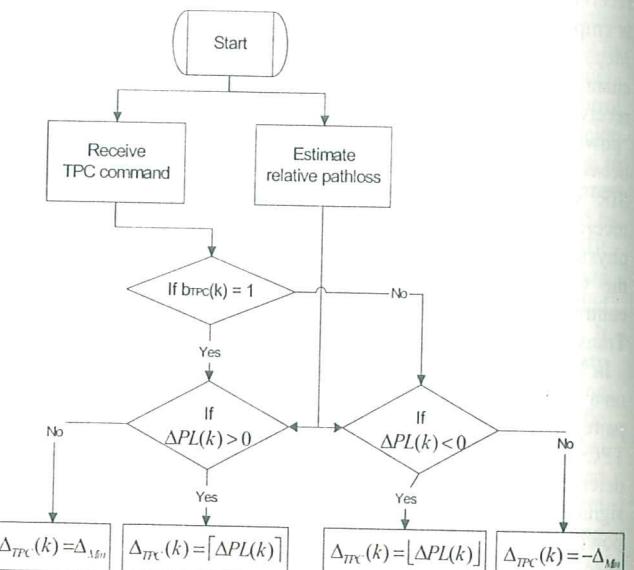


Figure 2. Flowchart of step size determination for the proposed closed loop power control

Since in the proposed scheme the transmitter varies the step size autonomously, the proposed scheme does not require additional feedback signaling bandwidth, as compared with [2]. However a reference physical channel is necessary for changing the step size. Taking into account the current 3G standards, the proposed scheme can be applied to uplink DPCHs for UTRA TDD and TD-SCDMA (Time Division-Synchronous Code Division Multiple Access) [11].

V. PERFORMANCE ANALYSIS

In this section, performance analysis of the current closed loop power control and proposed scheme is provided based on link-level simulations over various propagation channels. Table 4 lists the link-level simulation assumptions. Figure 3 depicts the timeslot configuration considered for the simulations.

Table 4. List of link-level simulation assumptions

Parameter	Assumption/Explanation
Chip rate	3.84 Mcps
Number of Information data bits per transport channel	512 bits
Power update rate	100 Hz (10 msec per update)
Number of codes and timeslots allocated to power controlled channel	7 codes and 1 timeslot per frame
Channel coding	Turbo coding with 4 turbo decoding iterations and Max-log MAP for SISO decoder
Puncturing rate	0 %
Modulation	QPSK
Channel estimation	Ideal
Receiver	MMSE multi-user detector (MUD)
Outer loop TPC	Off
Tx diversity	Off
Propagation condition	Case 1, Case 2, and VA 30
TPC command error rate	5 %

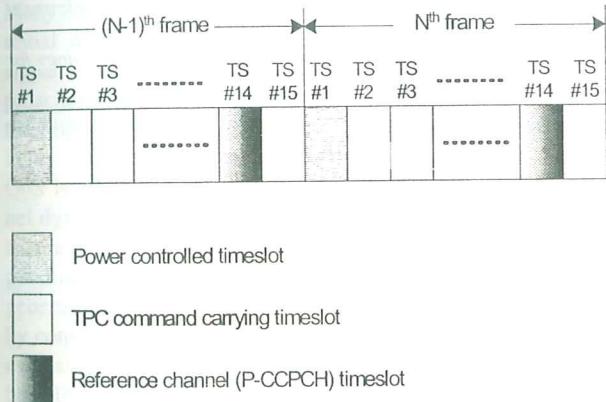


Figure 3. Timeslot configuration for power control simulations

The simulation results are summarized in Figures 5-7. Figures 5-6 are for mobile speed of 3km/h, while Figure 7 is for 30 km/h. Note that UTRA TDD is typically intended for applications in pico and micro cell environments with high density traffic and indoor coverage [9], implying low or moderate mobile speed environments. Figure 5 shows that in the existing closed loop using a fixed step size, the performance with a large step size (2 dB or 3 dB) is better than with the 1 dB step size under Case 1 channel. Under the same channel condition, the proposed pathloss aided closed loop power control provides a significant gain (more than 3 dB at BLER of 0.01) over the current closed loop using an optimal step size for the given channel. The performance advantage of the proposed power control scheme may be illustrated by Figure 4 presenting a sample distribution function of relative pathloss estimate reflecting the channel characterizing Case 1.

From Figure 4 and 5, it appears that as the propagation conditions dynamically vary in time, the proposed scheme is capable of adapting to the channel variations by adaptively changing the step size.

Similarly, Figure 6 shows that the proposed scheme outperforms the current closed loop using any fixed step size in Case 2 channel. Figure 7 presents the performance results over ITU vehicular A channel with a speed of 30 km/h. From the figure, it is observed that the performance of the proposed scheme is better than that of the current scheme. In addition, it can be seen that in the case of the current scheme, the performance with 1 dB step size is better than with 2 and 3 dB step sizes, respectively. Note however that the type of propagation channel is not known at the transmitter, so in addition to adapting to the variations in channel conditions, the proposed scheme adapts to changes in the propagation environment, i.e. whether the conditions reflect Case 1, 2 or 3, or any other propagation model.

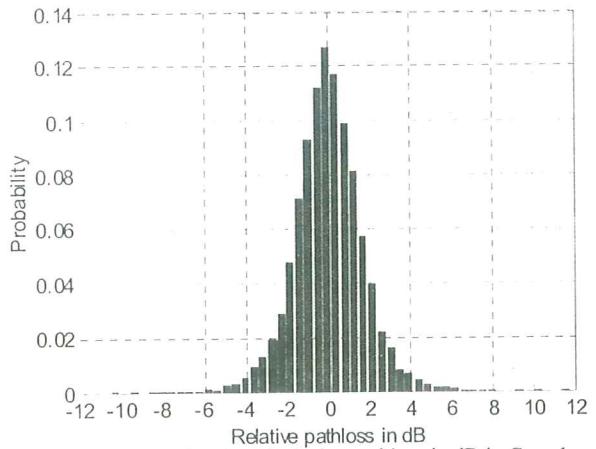


Figure 4. Distribution of relative pathloss in dB in Case 1

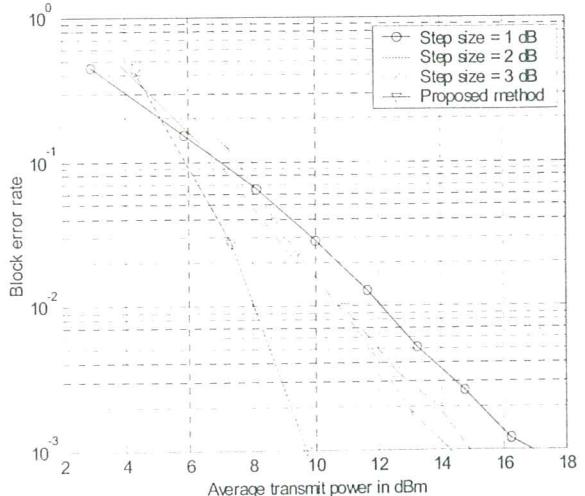


Figure 5. Block error rate vs. Tx power (dBm) for the existing closed loop TPC and proposed closed loop TPC under Case 1

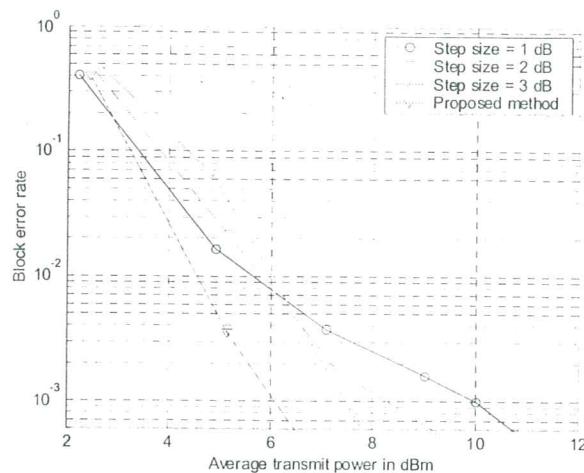


Figure 6. Block error rate vs. Tx power (dBm) for the existing closed loop TPC and proposed closed loop TPC under Case 2

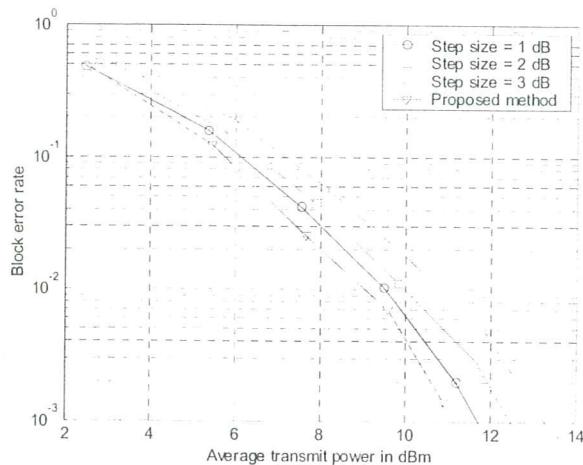


Figure 7. Block error rate vs. Tx power (dBm) for the existing closed loop TPC and proposed closed loop TPC under VA30

VI. CONCLUSIONS

In this paper, we have discussed the closed loop power control in UTRA TDD and proposed an enhanced (pathloss aided) closed loop power control scheme. The proposed scheme utilizes channel reciprocity and relative pathloss measurement to determine the power control step size, so that it can cope with rapid channel changes.

We studied the propagation channels specified in the standard and presented link level simulation results for the proposed power control scheme covering the various propagation channels. The simulation results show that the proposed closed loop power control scheme can offer substantial gains in the required transmit power over the current UTRA TDD closed loop power control scheme. These gains lead to significant improvements in TDD system capacity, in particular for slow and moderate fading channels.

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Table of Contents

Volume 1

Session 1A: Propagation/Channel Modeling 1 — UWB

1. New Channel Impulse Response Model for UWB Indoor System Simulations	1
Alvaro Alvarez, ACORDE SA, Spain;	
Gustavo Valera, Manuel Lobeira, Rafael Torres, Jose Luis Garcia, University of Cantabria, Spain	
2. A Wideband Dynamic Spatio-Temporal Markov Channel Model for Typical Indoor Propagation Environments	6
Chia-Chin Chong, David I. Laurenson, Stephen McLaughlin, University of Edinburgh, UK	
3. Transmission Coefficients Measurement of Building Materials for UWB Systems in 3-10 GHz	11
Ray-Rong Lao, Jenn-Hwan Tarn, National Chiao Tung University, Taiwan;	
Chiuder Hsiao, National Space Program Office, Taiwan	
4. Analysis of the Energy Dynamic of UWB Signal in Multi-Path Environments	15
Yongfu Huang, Xiangning Fan, Jiang Wang, Guangguo Bi, Southeast University, China	
5. Major Characteristics of UWB Indoor Transmission for Simulation	19
Michel Terré, Anton Hong, CNAM, France;	
Grégoire Guiibé, Fabrice Legrand, Thalès Communications, France	

Session 1B: MIMO 1 — Capacity

1. Correlation Number: A New Design Criterion in Multi-Antenna Communication	24
Angel Lozano, Lucent Technologies, USA;	
Antonia M. Tulino, Universita Degli Studi di Napoli, Italy;	
Sergio Verdu, Princeton University, USA	
2. Direction of Arrival and Capacity Characteristics of an Experimental Broadband Mobile MIMO-OFDM System	29
Thomas P. Krauss, Timothy A. Thomas, Frederick W. Vook, Motorola Labs, USA	
3. The Effect of Horizontal Array Orientation on MIMO Channel Capacity	34
Peter Almers, Telia Research AB, Sweden;	
Fredrik Tufvesson, Lund University, Sweden;	
Peter Karlsson, Telia Research AB, Sweden;	
Andreas F. Molisch, Lund University, Sweden	
4. Analysis of Different Precoding/Decoding Strategies for Multiuser Beamforming	39
Holger Boche, Martin Schubert, Heinrich-Hertz-Institut, Germany	
5. Capacity Autocorrelation Characteristic of MIMO Systems over Doppler Spread Channels	44
Chunyan Gao, Ming Zhao, Shidong Zhou, Yan Yao, Tsinghua Univ., China	

Session 1C: Space Time Coding 1

1. Multiple Trellis Coded Unitary Space-Time Modulation	47
Zhenyu Sun, National University of Singapore, Singapore;	
Tjeng Thiang Tjhung, Institute for Communications Research, Singapore	
2. High Speed Wireless Date Transmission in Layered Space-Time Trellis Coded MIMO Systems	52
Runhua Chen, George Washington University, USA;	
Khaled Ben Letaief, Hong Kong University of Science and Technology, Hong Kong	
3. Performance Evaluation of STTCs for Virtual Antenna Arrays	57
Mischa Dohler, Bilal Rassool, Hamid Aghvami, King's College London, UK	
4. A Design of Space-Time Trellis Code to Limit the Position of Received Symbols for MPSK	61
Susu Jiang, Ryuji Kohno, Yokohama National University, Japan	
5. Fast Search Techniques for Obtaining Space-Time Trellis Codes for Rayleigh Fading Channels and Its Performance in CDMA Systems	66
Bilal A. Rassool, F. Heliot, L. Revelli, M. Dohler, R. Nakhai, H. Aghvami, King's College London, UK	

Session 1D: Antenna (Smart Antenna) 1 — Capacity

1. Erlang Capacity of Smart Antenna CDMA System Considering the Sector Operation	70
Insoo Koo, KJIST, Korea;	
Seungchan Bang, Jeewan Ahn, ETRI, Korea;	
Kiseon Kim, KJIST, Korea	
2. On the Capacity of a Distributed Multiantenna System Using Cooperative Transmitters	75
Tobias J. Oechtering, Holger Boche, Technical University of Berlin, Germany	
3. Impact of the Base Station Antenna Beamwidth on Capacity in WCDMA Cellular Networks	80
Jarno Niemela, Jukka Lempainen, Tampere University of Technology, Finland	
4. Capacity Comparison of Multi-element Antenna Systems	85
Wanjun Zhi, National University of Singapore, Singapore;	
Francois Chin, Institute for Communications Research, Singapore;	
Chi Chung Ko, National University of Singapore, Singapore	
5. Capacity Evaluation of Transmit Beamforming CDMA System with FER Prediction Method	89
Cheol Yong Ahn, Young-Kwan Choi, Jin Kyu Han, Dong Ku Kim, Yonsei University, Korea	

Session 1E: CDMA System 1

1. Information-Theoretic Sum Capacity of Reverse Link CDMA Systems	93
Seong-Jun Oh, Aleksandar D. Damnjanovic, Anthony C.K. Soong, Ericsson Wireless Communication Inc. USA	
2. A Novel WCDMA Uplink Capacity and Coverage Model Including the Impact of Non-Ideal Fast Power Control and Macro Diversity	98
Kimmo Hiltunen, Ericsson Research, Finland;	
Magnus Karlsson, Ericsson Research, Sweden	
3. On the Capacity of Air-Ground W-CDMA System (Downlink Analysis)	103
Bazil Taha Ahmed, Miguel Calvo Ramón, Leandro Haro Ariet, UPM ETSI de Telecom., Spain	
4. On the Capacity and Interference Statistics of Street W-CDMA Cross-Shaped Micro Cells in Manhattan Environment (Uplink Analysis)	107
Bazil Taha Ahmed, Miguel Calvo Ramon, Leandro Haro Ariet, UPM ETSI de Telecom., Spain	
5. Uplink and Downlink SIR Analysis for Base Station Placement	112
Joseph K.L. Wong, Michael J. Neve, Kevin W. Sowerby, The University of Auckland, New Zealand	

Session 1F: OFDM 1 — OFCDM

1. Orthogonal Variable Spreading Factor Code Selection for Peak Power Reduction in Multi-Rate OFCDM Systems	117
Osamu Takyu, Keio University, Japan;	
Tomoaki Ohtsuki, Tokyo University of Science, Japan;	
Masao Nakagawa, Keio University, Japan	
2. OFCDM based Adaptive Modulation with Antenna Array in Fading Channels	122
Kapseok Chang, Youngnam Han, Information and Communications University, Korea	
3. Variable Spreading Factor-OFCDM with Two Dimensional Spreading that Prioritizes Time Domain Spreading for Forward Link Broadband Wireless Access	127
Noriyuki Maeda, Yoshihisa Kishiyama, Hiroyuki Atarashi, Mamoru Sawahashi, NTT DoCoMo Inc., Japan	
4. Fast Cell Search Algorithm for System with Coexisting Cellular and Hot-Spot Cells Suitable for OFCDM Forward Link Broadband Wireless Access	133
Motohiro Tanno, Hiroyuki Atarashi, Kenichi Higuchi, Mamoru Sawahashi, NTT DoCoMo, Japan	
5. Investigation of Optimum Pilot Channel Structure for VSF-OFCDM Broadband Wireless Access in Forward Link	139
Yoshihisa Kishiyama, Noriyuki Maeda, Hiroyuki Atarashi, Mamoru Sawahashi, NTT DoCoMo Inc., Japan	

Session 1G: TDMA System 1 — Resource Management

1. Traffic Control Algorithms for a Multi Access Network Scenario Comprising GPRS and UMTS	145
Filippo Malavasi, Michele Breveglieri, Luca Vignali, Ericsson Telecommunicazioni, Italy;	
Paul Leaves, University of Surrey, UK;	
Jorg Huschke, Ericsson Eurolab, Germany	
2. Optimization of Handover Margins in GSM/GPRS Networks	150
Matias Toril, University of Malaga, Spain;	
Salvador Pedraza, Ricardo Ferrer, Volker Wille, Nokia Networks, Spain	

3. Dimensioning of Signaling Capacity on a Cell Basis in GSM/GPRS	155
Salvador Pedraza, Volker Wille, Nokia Networks, Spain;	
Matias Toril, University of Malaga, Spain;	
Ricardo Ferrer, Juan J. Escobar, Nokia Networks, Spain	
4. Modeling and Analysis of Combined Mobility Management Based on Implicit Cell Update Scheme in General Packet Radio Service	160
Yun Won Chung, Dan Keun Sung, Korea Advanced Institute of Science and Technology, Korea	
5. Scalable Resource Allocation Algorithm for GPRS	165
S. Tang, Rahim Tafazolli, University of Surrey, UK	

Session 1H: WLAN/Ad Hoc Network 1 — Multihop Network

1. Average Outage Duration of Multihop Communication Systems with Regenerative Relays	171
Lin Yang, Mazen O. Hasna, Mohamed-Slim Alouini, University of Minnesota, USA	
2. Time and Message Complexities of the Generalized Distributed Mobility-Adaptive Clustering (GDMAC) Algorithm in Wireless Multihop Networks	176
Christian Bettstetter, Bastian Friedrich, Technische Universitat Munchen, Germany	
3. An Analysis of Mobile Radio Ad Hoc Networks Using Clustered Architectures	181
Mattias Skold, Swedish Defence Research Agency, Sweden;	
Yeongyang Choi, Korea Military Academy, Korea;	
Jan Nilsson, Swedish Defence Research Agency, Sweden	
4. Multi-step Increase of the Forwarding Zone for LAR Protocol in Ad Hoc Networks	186
F. De Rango, University of Calabria, Italy;	
A. Iera, University of Reggio Calabria, Italy;	
A. Molinaro, S. Marano, University of Calabria, Italy	
5. Hybrid Gateway Advertisement Scheme for Connecting Mobile Ad Hoc Networks to the Internet	191
JeongKeun Lee, Seoul National University, Korea;	
Dongkyun Kim, Kyungpook National University, Korae;	
J.J. Garcia-Luna-Aceves, University of California at Santa Cruz, USA;	
Yanghee Choi, Seoul National University, Korea;	
Jihyuk Choi, Sangwoo Nam, Electronics and Telecommunications Research Institute, Korea	

Poster Session 1: Propagation/Channel Modeling

1. Propagation Model for the WLAN Service at the Campus Environments	196
Ki Hong Kim, Jung Ha Kim, Young Joong Yoon, Yonsei University, Korea;	
Jae Ho Seok, Jae Woo Lim, RRL, Korea	
2. A Study of 2.3GHz bands Propagation Characteristic Measured in Korea	201
Ho-Kyung Son, ETRI, Korea;	
Geun-Sik Bae, Agency for Defense Development, Korea;	
Hung-Soo Lee, ETRI, Korea	
3. Application of Isolated Diffraction Edge (IDE) Method for Urban Microwave Path Loss Prediction	205
Hyun Kyu Chung, ETRI, Korea;	
Henry L. Bertoni, Polytechnic University, USA	
4. A Quadrant-Based Range Location Method	210
Qun Wan, Shen-Jian Liu, Feng-Xiang Ge, Jing Yuan, Ying-Ning Peng, Tsinghua University, China;	
Wan-Lin Yang, University of Electronic Science and Technology of China, China	
5. DOA Estimator for Multiple Coherently Distributed Sources with Symmetric Angular Distribution	213
Qun Wan, Shen-Jian Liu, Feng-Xiang Ge, Jing Yuan, Ying-Ning Peng, Tsinghua University, China;	
Wan-Lin Yang, University of Electronic Science and Technology of China, China	
6. A Generic Channel Model in Multi-cluster Environments	217
Yifan Chen, Vimal K. Dubey, Nanyang Technological University, Singapore	
7. On the Frequency Dependence of Wireless Propagation Channel's Statistical Characteristics	222
Z. Irahhauten, H. Nikookar, Delft University of Technology, Netherland	
8. Static and Dynamic Radio Channel Models for LMDS System	227
P. Soma, L.C. Ong, S. Sun, Y.W.M Chia, Institute for Infocomm Research, Singapore	
9. The LR2 Model for Mobile Satellite Channels and its System Performance Analysis	231
Xing Li, Shiqi Wu, University of Electronic Science & Technology of China, China	

Session 2A: Propagation/Channel Modeling 2

1. Accurate and Efficient Prediction of Coverage Map in an Office Environment Using Frustum Ray Tracing and in-Situ Penetration Loss Measurement	236
Hajime Suzuki, CSIRO, Australia	
2. An Exact Analysis of the Impact of Fading Correlation on the Average Level Crossing Rate and Average Outage Duration of Selection Combining	241
Lin Yang, Mohamed-Slim Alouini, University of Minnesota, USA	
3. Directional Measurement and Analysis of Propagation Path Variations in a Street Micro-Cell Scenario	246
Andreas Richter, Reiner S. Thomae, Ilmenau University of Technology, Germany; Tokio Taga, NTT DoCoMo, Japan	
4. Influence of the Human Activity on the Propagation Characteristics of 60 GHz Indoor Channels	251
Sylvain Collonge, Gheorghe Zaharia, Ghais El zein, Institute of Electronic and Telecommunication of Rennes, France	
5. System Functions and Characteristic Quantities of Spatial Deterministic Gaussian	256
Uncorrelated Scattering Processes Matthias Patzold, Agder University College, Norway	

Session 2B: MIMO 2 — Signal Processing

1. Optimal Multi-User MISO Solution with Application to Multi-User Orthogonal Space Division Multiplexing	262
Zhengang Pan, Kai-Kit Wong, Tung-Sang Ng, University of Hong Kong, Hong Kong	
2. Statistical Prefiltering for MIMO Systems with Linear Receivers in the Presence of Transmit Correlation	267
Mario Kiessling, Joachim Speidel, University of Stuttgart, Germany; Ingo Viering, Markus Reinhardt, Siemens AG, Germany	
3. MIMO Equalization for Space-Time Coded Signals Using Cyclostationarity	272
Jinho Choi, University of New South Wales, Australia	
4. A Computationally Efficient MIMO Turbo-Equaliser	277
Kimmo Kansanen, Tad Matsumoto, University of Oulu, Finland	
5. Limitations in Spectral Efficiency of a Rate-Adaptive MIMO System Utilizing Pilot-Aided Channel Prediction	282
Bengt Holter, Geir E. Oien, Kjell J. Hole, Henrik Holm, Norwegian University of Science and Technology, Norway	

Session 2C: Space Time Coding 2

1. Partial Feedback Based Orthogonal Block Coding	287
Jabran Akhtar, David Gesbert, University of Oslo, Norway	
2. Triangular Non-Orthogonal Space-Time Block Code	292
Rong Ran, Jia Hou, Moon Ho Lee, Chonbuk National University, Korea	
3. Full-Rate Full-Diversity STBC with Constellation Rotation	296
Chau Yuen, Yong Liang Guan, Nanyang Technological University, Singapore; Tjeng Thiang Tjhung, Institute of Communication Research, Singapore	
4. A Robust Non-Orthogonal Space-Time Block Code for Four Transmit Antennas	301
Fu-Chun Zheng, Alister G. Burr, University of York, UK	
5. A New Differential Space-Time Block Coding Scheme for Two, Three and Four Transmit Antennas	306
Xun Shao, Jinhong Yuan, University of New South Wales, Australia; Branka Vucetic, University of Sydney, Australia	

Session 2D: Antenna (Smart Antenna) 2 — Downlink Performance

1. Increasing the Peak Data Rate of 3G Downlink Packet Data Systems Using Multiple Antennas	311
Howard Huang, Sivarama Venkatesan, Achilles Kogiantis, Naresh Sharma, Lucent Technologies, USA	
2. Comparison of Antenna Array Techniques for the Downlink of Multi-Carrier CDMA Systems	316
Thomas Salzer, David Mottier, Damien Castelain, Mitsubishi Electric ITE, France	
3. Down-Link Channel Modeling for Mobile Communications with Smart Antennas at the Base Station	321
Qi Yao, Matthias Patzold, Agder University College, Norway	
4. On the Performance of Beam-Tracking Antennas for Downlink Layer Separation in Multi-Layer CDMA Cellular Systems	326
S.A. Ghorashi, L. Wang, F. Said, A.H. Aghvami, King's College London, UK	
5. Joint Downlink Beamforming and Power Control for 3G WCDMA	331
Martin Schubert, Dimitrios Karadoulamas, Holger Boche, Heinrich-Hertz-Institute, Germany; Gerald Lehmann, Siemens AG, Germany	

Session 2E: CDMA System 2

1. Effect of Physical Layer Bandwidth Variations on TCP Performance in CDMA2000	336
Etienne Chaponnier, Sunil Kandukuri, Walid Hamdy, Qualcomm Inc., USA	
2. Interference Power Variation in Integrated Services CDMA Networks: A Single Cell Analysis	343
Alagan Anpalagan, Ryerson University, Canada	
3. Performance of DS-CDMA System with Smart Antenna for Different Bandwidths in the Wideband Multipath Channel	348
Jun-Soo Jeon, Jeong-Won Lee, Cheol-Sung Kim, Chonnam Naional University, Korea	
4. Experiences with Video Conferencing over CDMA2000	352
Arif Khan, Walid Hamdy, Sunil Kandukuri, Qualcomm Inc., USA	
5. Optimal Decoding Order and Power Allocation in Multimedia CDMA Networks with Imperfect Successive Interference Cancellation	358
Tao Shu, Zhisheng Niu, Tsinghua University, China	

Session 2F: OFDM 2 — Receiver (1)

1. Asymptotic Analysis of the Multiuser MMSE Receiver for the Downlink of a MC-CDMA System	363
Pierre Jallon, M. des Noes, D. Ktenas, CEA, France;	
Jean-Marc Brossier, LIS, France	
2. An OFDM Receiver with Decision-Directed Channel Estimation for the Scattered Pilot Scheme in Fast Fading Environments	368
Masafumi Ito, Satoshi Suyama, Kazuhiko Fukawa, Hiroshi Suzuki, Tokyo Institute of Technology, Japan	
3. Design Criteria for Phase Sequences in Selected Mapping	373
Naoto Ohkubo, Tomoaki Ohtsuki, Tokyo University of Science, Japan	
4. OFDM Timing Synchronisation under Multi-path Channels	378
N. Chen, M. Tanaka, R. Heaton, Mitsubishi Electric ITE B.V., UK	
5. A Study on MMSE Combining for MC-CDMA	383
Isao Sato, Teruya Fujii, Japan Telecom Co., Ltd., Japan	

Session 2G: TDMA System 2

1. Performance Analysis of Channel Rate Selection Schemes in Systems with Tight Reuse	388
Krishna Balachandran, Tingfang Ji, Joseph H. Kang, James P. Seymour, Lucent Technologies, Bell Laboratories, USA	
2. Intra-System Load Balancing between Adjacent GSM Cells	393
Antti Tolli, Nokia Networks, Spain;	
Isabel Barbancho, University of Malaga, Spain;	
Juan Gomez, Petteri Hakalin, Nokia Networks, Spain	
3. Forward Link Capacity of Overlaid Multiclass CDMA Systems and TDMA Systems with Slots Reallocation on the TDMA Layer	398
Josefina Castaneda-Camacho, Domingo Lara-Rodriguez, Cinvestav, Mexico	
4. IP Multimedia Services Improvements in the GSM/EDGE Radio Access Network	403
Benoist Sebire, Nokia Research Center, Finland;	
Tommy Bysted, Kent Pedersen, Nokia Mobile Phones, Denmark	
5. Enhancing GSM Capacity in the Indoor Environment Using the nanoBTS	408
Mauro Fiacco, Neil Piercy, Ip access Ltd, UK	

Session 2H: WLAN/Ad Hoc Network 2 — Energy

1. Power and Rate Adaptation in IEEE802.11a Wireless LANs	413
Jens Jelitto, Andre Noll Barreto, Hong Linh Truong, IBM Research, Switzerland	
2. Time and Energy Efficient Service Discovery in Bluetooth	418
Igor Sedov, Stephan PreuB, Clémens Cap, Marc Haase, Dirk Timmermann, University of Rostock, Germany	
3. Power Controlled Multiple Access control for Wireless Access Nets	423
Arash Behzad, Izhak Rubin, University of California (UCLA), USA	
4. Energy-Efficient Routing in DSSS Ad Hoc Networks under Mean Rate Constraints	428
Riku Jantti, University of Vaasa, Finland;	
Seong-Lyun Kim, Information and Communications University, Korea	
5. Adaptive Transmit Power Control in IEEE 802.11a Wireless LANs	433
Daji Qiao, University of Michigan, USA;	

Poster Session 2: Radio Resource Management (RRM)

1. Resource Reservation in Call Admission Control Schemes for CDMA Systems with Non-uniform Traffic Distribution among Cells	438
Insoo Koo, Seungjae Bahng, Kiseon Kim, KJIST, Korea	
2. Call Admission Scheme Using Ranking New Calls According to Total Resource Requirements in CDMA Systems	442
Shi Quan Piao, Yong Wan Park, Yeungnam University, Korea	
3. QoS Provisioning in Domain Based Mobile IP Networks	447
J. M. Moon, M. Y. Yun, ETRI, Korea;	
G.S. Park, ADD, Korea;	
K.I. Kim, Y.J. Kim, S.H. Kim, Chungnam National Univ., Korea	
4. Adaptive Filtering Applied to an Uplink Load Estimate in WCDMA	452
Erik Geijer Lundin, Fredrik Gunnarsson, Fredrik Gustafsson, Linkopings Universitet, Sweden	
5. A 2-Level Call Admission Control Scheme Using Priority Queue for Decreasing New Call Blocking & Handoff Call Dropping	457
Myung Il Kim, Sung Jo Kim, Chung-Ang University, Korea	
6. Scheduling of Real/Non-Real Time Services: Adaptive EXP/PF Algorithm	462
Jong-Hun Rhee, Yonsei University, Korea;	
Jack M. Holtzman, Qualcomm Incorporated, USA;	
Dong-Ku Kim Yonsei University, Korea	
7. Scheduling Based on Message in Ad Hoc Networks	467
Tian Hui, Xie Fang, Li YingYang, Hu JianDong, Zhang Ping, Beijing University of Posts & Telecommunications, China	
8. A Simple Minimum Rate Supporting Scheduler for UTRA/TDD High Speed Downlink Packet Access	472
Dongwoo Kim, Hanyang University, Korea;	
Dong Seung Kwon, Sung Kyung Kim, ETRI, Korea	
9. A Channel-Adaptive and Throughput-Efficient Scheduling Scheme in Power-Constrained Voice/Data CDMA Networks Based on Ranking of Received Power Capabilities	476
Tao Shu, Zhisheng Niu, Tsinghua University, China	
10. A MAC Protocol with Efficient Fair Scheduling for CDMA-Based Mobile Networks	481
Liang Zhang, Tony T. Lee, The Chinese University of Hong Kong, Hong Kong	
11. The Handoff Schemes in Mobile IP	485
Liu Yu, Ye Min-hua, Zhang Hui-min, Beijing University of Posts and Telecommunications, China	
12. Outer Loop Power Control Using Channel-Adaptive Processing for 3G WCDMA	490
Chang-Soo Koo, Sung-Hyuk Shin, Robert A. DiFazio, Donald Grieco, Ariela Zeira, InterDigital Communications Corp., USA	
13. Adaptive Power/Rate Allocation for Minimum Mean Transmission Delay in CDMA Networks	495
Kwonhue Choi, Sooyoung Kim, ETRI, Korea	
14. Performance of 2-bit Power Control Algorithm in CDMA Networks under Rayleigh Fading: A Comparative Simulation Study	500
Naeem Sahi, Alagan Anpalagan, Ryerson University, Canada	
15. A CDMA Based Scheduling Algorithm with IP QoS Guarantee	505
Cui Chunfeng, Du Lei, Zhang Ping, Beijing University of Posts & Telecommunications, China	

Session 3A: Propagation/Channel Modeling 3

1. Methods of Generating Multiple Uncorrelated Rayleigh Fading Processes	510
Cheng-Xiang Wang, Matthias Pätzold, Agder University College, Norway	
2. An Efficient Context Tree Based Model for RAKE and Flat Fading Channel	515
Ahmed saadani, Pierre Gelpi, Patrick Tortelier, FranceTelecom R&D, France	
3. Fast DOA Estimation Algorithm Using Pseudo Covariance Matrix	519
Jung-Tae Kim, Dong-Seog Han, Kyungpook National University, Korea	
4. A New Hidden Markov Model for Very Bursty Channels	524
Weiling Zhu, Javier Garcia-Frias, University of Delaware, USA	
5. Joint Estimation of Propagation Delay and Direction of Arrival of Multipath Signals	529
Alongkot Pholyiam, Kazi M. Ahmed, Asian Institute of Technology, Thailand;	
Hiroyuki Tsuji, Communications Research Laboratory, Japan;	
W.A.C.Fernando, Asian Institute of Technology, Thailand	

Session 3B: MIMO 3 — Channel Model

1. Effect of Far Scatterer Clusters in MIMO Outdoor Channel Models	534
Andreas F. Molisch, Mitsubishi Electric Research Labs, USA	
2. Performance Analysis of a Channel Oriented Concept for Multi-User MIMO Downlinks with Frequency Selective Channels	539
Wei Qiu, Hendrik Tröger, Michael Meurer, Christoph A. Jöttgen, University of Kaiserslautern, Germany	
3. Characterisation of the Time-Dependent Urban MIMO Channel in FDD Communication Systems	544
Juergen Maurer, Christian Waldschmidt, Thorsten Kayser, Werner Wiesbeck, University of Karlsruhe, Germany	
4. Matched Filter Bound for Space-Time Block Coded MIMO Systems in Correlated Multipath Fading	549
Hafez Hadinejad-Mahram, Aachen University of Technology, Germany; Dirk Dahlhaus, Swiss Federal Institute of Technology Zurich, Swiss	
5. Simple Capacity Formulas for Correlated SIMO Nakagami Channels	554
Q. T. Zhang, City University of Hong Kong, Hong Kong; D. P. Liu, Beijing University of Posts and Telecommunications, China	

Session 3C: Space Time Coding 3

1. Space-Frequency Trellis Coding for MIMO OFDM Systems	557
Zihua Guo, Wenwu Zhu, Microsoft Research Asia, China; Khaled Ben Letaief, Hong Kong Univ. of Science & Technology, Hong Kong	
2. Variable-Rate OFDM Systems with Selective Antenna Diversity and Adaptive Modulation	562
Mohammad Torabi, M. Reza Soleymani, Concordia University, Canada	
3. Space-Time Block Codes Versus Space-Frequency Block Codes	567
Gerhard Bauch, DoCoMo Euro-Labs, Germany	
4. Matrices Analysis Based on Jacket for Space Time Block Codes	572
Jia Hou, Moon Ho Lee, Chonbuk National University, Korea; Ju Yong Park, Seonam University, Korea	
5. Space-Time Block Coding Applied to Turbo Coded Multicarrier CDMA	577
Vincent Le Nir, Maryline Helard, Rodolphe Le Gouable, France Telecom R&D, France	

Session 3D: Antenna (Smart Antenna) 3

1. Implementation of Smart Antenna Base Station for IS-2000 1X	582
HeungJae Im, Seungheon Hyeon, Weon-cheol Lee, Hanyang University, Korea; Hwanseog Bahk, Cheolhoon Lee, Jonghun Kim, Hantel Co., Ltd., Korea; Seungwon Choi, Hanyang University, Korea	
2. Performance of the Distributed Antenna Systems in a Multi Cell Environment	587
Wonil Roh, Argyyaswami Paulraj, Stanford University, USA	
3. Partially Adaptive Beamformers via Wavelet-Based Subband Decomposition	592
Wen-Hsien Fang, He-Mo Hung, National Taiwan University of Science and Technology, Taiwan	
4. A Simple Null-Steering Adaptive Array Antenna in OFDM-Based WPAN/WLAN	597
Shinsuke Hara, Shuichi Hane, Yunjian Jia, Osaka University, Japan	
5. Multipath Mitigation Technique Using Null-Steering Beamformer for Positioning System	602
Seungyeun Yoo, Sangheon Kim, Dae Hee Youn, Chungyong Lee, Yonsei University, Korea	

Session 3E: CDMA System 3

1. On the Network Performance of UTRA-like TDD and FDD CDMA Systems Using Adaptive Modulation and Adaptive Beamforming	606
Song Ni, Jonathan S. Bloch, Lajos Hanzo, University of Southampton, UK	
2. TCP Performance Analysis in Wireless Transmission Using AMC	611
Kae Won Choi, Wha Sook Jeon, Seoul National University, Korea; Dong Geun Jeong, Hankuk University of Foreign Studies, Korea	
3. Throughput Comparison of Random Access Schemes in 3GPP	616
Ivan N. Vukovic, Motorola Inc., USA	
4. A TCP-friendly Congestion Control Algorithm for 1xEV-DV Forward Link Packet Data	621
Patrick Hosein, Ericsson Wireless Communications, Inc., USA	
5. Impact of TCP and RLP Parameters on CDMA2000 Performance	626
Sunil Kandukuri, Etienne Chaponniere, Walid Hamdy, Qualcomm Inc., USA	

Session 3F: OFDM 3 — Receiver (2)

1. An OFDM Receiver Employing Turbo Equalization for Multipath Environments with Delay Spread Greater than the Guard Interval	632
Satoshi Suyama, Hiroshi Suzuki, Kazuhiko Fukawa, Tokyo Institute of Technology, Japan	
2. Iterative Detection for Walsh-Hadamard Transformed OFDM	637
Zhongding Lei, Yan Wu, Chin Keong Ho, Sumei Sun, Ping He, Yuan Li, Institute for Infocomm Research, Singapore	
3. Pre-Filtering Antenna Array for Downlink TDD MC-CDMA Systems	641
Adao Silva, Atilio Gameiro, Institute of Telecommunications, Portugal	
4. Coarse Timing Recovery in Burst Mode OFDM	646
Ha H. Nguyen, J. Eric Salt, Zhiyi Zhou, University of Saskatchewan, Canada	
5. Time versus Frequency Domain Channel Tracking Using Kalman Filters for OFDM Systems with Antenna Arrays	651
Zhenlan Cheng, Dirk Dahlhaus, ETH Zurich, Switzerland	

Session 3G: Multimedia Traffic

1. Cost Function for Resources Allocations in a Radio Packet Communication Network	656
Emmanuelle Vivier, ISEP, France;	
Michel Terre, Demba Cisse, Bernard Fino, CNAM, France	
2. Traffic Model for Multimedia Mobile Radio Communications	661
Shinya Hirachi, Shigeaki Ogose, Kagawa University, Japan	
3. A MAC Protocol Supporting Multiple Traffic over Mobile Ad Hoc Networks	665
Tian Hui, Li YingYang, Hu JianDong, Zhang Ping, Beijing University of Posts & Telecommunications, China	
4. Variable-Bit-Rate Traffic Modelling for Dimensioning 3G CDMA Systems	670
Brad C. Sowden, Kevin W. Sowerby, The University of Auckland, New Zealand	
5. Buffer Management for Rate-Varying 3G Wireless Links Supporting TCP Traffic	675
Mats Sagfors, Oy LM Ericsson, Finland;	
Reiner Ludwig, Michael Meyer, Ericsson Research, Germany;	
Janne Peisa, Oy LM Ericsson, Finland	

Session 3H: WLAN/Ad Hoc Network 3 — Heterogeneous System Overlay

1. An Investigation of the Impact of Bluetooth Interference on the Performance of 802.11g Wireless Local Area Networks	680
Angela Doufexi, Arun Arumugam, Simon Armour, Andrew Nix, University of Bristol, UK	
2. Simulation Study of IEEE 802.11e EDCF	685
Daijiang He, Charles Q. Shen, National University of Singapore, Singapore	
3. 802.11g CP: A Solution for IEEE 802.11g and 802.11b Inter-Working	690
Sunghyun Choi, Seoul National University, Korea;	
Javier del Prado Pavon, Philips Research USA, USA	
4. Mobile Communication Systems with Multi-Layered Wireless Network Using Ad Hoc Network	695
Shigeaki Ogose, Shindoh Sasaki, Kazumasa Itoh, Kagawa University, Japan	
5. A Multidisciplinary Study of Competition in Unlicensed Networks	699
Olav Queseth, KTH/S3/Radio, Sweden	

Poster Session 3: Space Time Coding & MIMO

1. Use of Space Time Block Codes and Spatial Multiplexing using TDLS Channel Estimation to Enhance the Throughput of OFDM Based WLANs	704
Angela Doufexi, Arantxa Prado Miguelez, Simon Armour, Andrew Nix, Mark Beach, University of Bristol, UK	
2. Delay Estimation for Space-Time Coded Signals over Rayleigh Fading Channels	709
Sang-Min Lee, Dong-Jo Park, Yeong-Hyeon Kwon, Korea Advanced Institute of Science and Technology, Korea	
3. Signal Constellations for Differential Unitary Space-Time Modulation with Multiple Transmit Antennas	713
Cheng Shan, A. Nallanathan, Pooi Yuen Kam, National University of Singapore, Singapore	
4. Interference Suppression Schemes for Space-Time Trellis Coded WCDMA Systems	717
Hayoung Yang, Samsung Electronics Co., Ltd., Korea;	
Jinhong Yuan, University of New-South Wales, Australia;	
Branka Vucetic, the University of Sydney, Australia;	
5. Effect of Imperfect Channel Information on M-QAM SER Performance of Orthogonal Space-Time Block Codes	722
Eunseok Ko, Changeon Kang, Daesik Hong, Yonsei Univ., Korea	

6. Improved Space-Time Turbo Codes with Full Spatial Diversity over Integer Ring	727
Tae Min Kim, Jae Hong Lee, Seoul National University, Korea	
7. Coordinate-Interleaved Space-Time Coding with Rotated Constellation	732
Young-Hak Kim, Mostafa Kaveh, University of Minnesota, USA	
8. Serial Concatenation Schemes for Space-Time and Recursive Convolutional Codes	736
Young-Jo Ko, Jung-Im Kim, ETRI, Korea	
9. The Performance of Space-Time Codes in Office Environments	741
Steve Parker, Magnus Sandell, Michele Lee, Toshiba Research Europe Limited, UK	
10. Performance Analysis of Serial Concatenated Space-Time Code in OFDM over Frequency Selective Channels	746
P. Patcharamanepakorn, Asian Institute of Technology, Thailand;	
R.M.A.P. Rajatheva, University of Moratuwa, Sri Lanka;	
Kazi Ahmed, Asian Institute of Technology, Thailand	
11. Comparison of Three Closed-loop Transmit Diversity Schemes	751
Zhuo Chen, Branka Vucetic, University of Sydney, Australia;	
Jinhong Yuan, University of New South Wales, Australia	
12. SIC-Based Decoding Algorithm for Space-Frequency Coded Transmitter Diversity	755
Bin Xu, Chenyang Yang, Shiyi Mao, Beijing University of Aeronautics and Astronautics, China	
13. Space-Time MMSE Multiuser Receiver for Space-Time Coded DS/CDMA Systems in Frequency Selective Fading Channels	759
Hyeon Chyeol Hwang, Kyung Sup Kwak, Inha University, Korea	
14. OFDM-CDM with V-BLAST Detection and its Extension to MIMO Systems	764
Kilsik Ha, Kwang Bok Lee, Seoul National University, Korea	
15. An Adaptive Channel SVD Tracking Strategy in Time-Varying TDD System	769
Ying Tan, Guillaume Lebrun, Mike Faulkner, Victoria University of Technology, Australia	
16. Adaptive Rate MIMO System Using Space-Time Block Mapping	774
Kyu Jong Hwang, Sok-Kyu Lee, Kyung Hi Chang, ETRI, Korea	
17. Information-Theoretic Capacity Analysis in MIMO Distributed Antenna Systems	779
Liang Xiao, Lin Dai, Hairuo Zhuang, Shidong Zhou, Yan Yao, Tsinghua University, China	

Volume 2

Session 4A: Propagation/Channel Modeling 4

1. A New Heuristic UTD Diffraction Coefficient for Prediction of Radio Wave Propagation	783
Hassan M. El-Sallabi, Pertti Vainikainen, Helsinki University of Technology, Finland	
2. Improvement in a Heuristic UTD Diffraction Coefficient for Prediction of Radio Wave Propagation	788
Hassan El-Sallabi, Pertti Vainikainen, Helsinki University of Technology, Finland	
3. Spatial Temporal Characterization of UTRA FDD Channels at the User Equipment	793
S.E. Foo, C.M. Tan, M.A. Beach, University of Bristol, UK	
4. Global Shadowing Margins for 3G Networks	798
Alban Durrenbach, Benoît Fourestié, Maryna Rault, Sylvain Renou, France Telecom R&D, France	
5. Stochastic Modeling and Simulation of Frequency Hopping Wideband Fading Channels	803
Cheng-Xiang Wang, Matthias Pätzold, Qi Yao, Agder University College, Norway	

Session 4B: MIMO 4

1. The Dependency of Turbo MIMO Equalizer Performance on the Spatial and Temporal Multipath Channel Structure – A Measurement Based Evaluation	808
Christian Schneider, Reiner Thomä, Technische Universität Ilmenau, Germany;	
Uwe Trautwein, Tewisoft GmbH, Germany;	
Tad Matsumoto, University of Oulu, Finland	
2. Bit-Allocation Strategies for MIMO Fading Channels with Channel Knowledge at Transmitter	813
Joon Hyun Sung, John R. Barry, Georgia Institute of Technology, USA	
3. System Architecture and ASICs for a MIMO 3GPP-HSDPA Receiver	818
L.M. Davis, D. C. Garrett, G. K. Woodward, M. A. Bickerstaff, Lucent Technologies, Australia;	
F. J. Mullany, Lucent Technologies, UK	
4. Weight Control Scheme for MIMO System with Multiple Transmit and Receive Beamforming	823
Yoshitaka Hara, Akinori Taira, Takashi Sekiguchi, Mitsubishi Electric Corporation, Japan	
5. Joint Transmitter-Receiver Optimization for Multiple Input Multiple Output (MIMO) Systems	828
Keun Chul Hwang, Kwang Bok (Ed) Lee, Seoul National University, Korea	

Session 4C: Space Time Coding 4

1. Maximum Diversity Detection for Layered Space-Time Codes	833
Aydin Sezgin, Eduard A. Jorswieck, Volker Jungnickel, Heinrich-Hertz-Institut, Germany	
2. Simple Correlation Canceling Algorithm for Space Time Block Codes	838
Jia Hou, Moon Ho Lee, Chonbuk National University, Korea;	
Ju Yong Park, Seonam University, Korea	
3. Comparison of Suboptimal Iterative Space-Time Receivers	842
Arnaud Gueguen, Mitsubishi Electric ITE, France	
4. Improved Iterative EM Receiver for Space Time Coded Systems in Frequency Selective Fading Channel with Channel Gain and Order Estimation	847
Daniel Ka Chun So, Roger S. Cheng, Hong Kong University of Science and Technology, Hong Kong	
5. Constrained Mean-Square-Error Space-Time Pre-Equalizer for the Downlink Channel of UMTS-TDD	852
A. Morgado, A. Gameiro, J. Fernandes, University of Aveiro, Portugal	

Session 4D: Antenna (Smart Antenna) 4

1. A Reconfigurable Electrically-Small Antenna Operating in the 'DC' Mode	857
P.R. Urwin-Wright, G.S. Hilton, I.J. Craddock, P.N. Fletcher, University of Bristol, UK	
2. Link Adaptation in a Multi-Antenna System	862
Volker Jungnickel, Thomas Haustein, Volker Pohl, Clemens von Helmolt, Heinrich-Hertz-Institut, Germany	
3. Model Based Antenna Array Calibration for Digital Beamforming Systems	867
Hyung Geun Park, Seung Chan Bang, Electronics and Telecommunication Research Institute, Korea	
4. A Novel SDMA Configuration Using Smart Antenna Adopting Vertical Pattern and Polarization Control	871
Kentaro Nishimori, Keizo Cho, NTT Corporation, Japan	
5. The Performance of Feedback Type Adaptive Array Antenna in FDD/DS-CDMA System	876
Mona Shokair, Yoshihiko Akaiwa, Kyushu University, Japan	

Session 4E: CDMA System 4

1. Network Effect of WCDMA Compressed Mode	881
Seppo Hämäläinen, Nokia Research Center, China;	
Tero Henttonen, Nokia Research Center, Finland;	
Jussi Numminen, Jukka Vikstedt, Nokia Mobile Phones, Finland	
2. Performance of DS-CDMA Systems with Band Limitation and Narrow-Band Rejection Filters	886
Yu Jiang, Hiroji Kusaka, Oskaka Sangyo Univ., Japan;	
Masanobu Kominami, Oskaka Electo-Commun.Univ, Japan	
3. Performance Improvement of Correlation-Flattened Binary CDMA	891
Yong Cheol Kim, Minwoo Chong, University of Seoul, Korea	
4. Performance Improvement with Fast Site Switching in a CDMA Forward Link	896
Hichan Moon, Donald C. Cox, Stanford University, USA	
5. Performance Evaluation of CPCH with a Geometrically-Distributed Message Length in W-CDMA	901
Moon Young Choi, Yu-Dong Yao, Harry Heffes, Stevens Institute of Technology, USA	

Session 4F: OFDM 4 — AMC

1. Adaptive Subcarrier and Power Allocation in OFDM Based on Maximizing Utility	905
Guocong Song, Ye (Geoffrey) Li, Georgia Institute of Technology, USA	
2. Proposal of Adaptive Subchannel and Bit Allocation Method for OFDM Access Wireless LAN Systems	910
Yuanrun Teng, Tomotaka Nagaosa, Kazuo Mori, Hideo Kobayashi, Mie University, Japan	
3. On the Optimal Discrete Bit Loading for Multicarrier Systems with Constraints	915
Antonio Fasano, University of Roma "La Sapienza," Italy	
4. Enhanced Link Adaptation Performance Applying Adaptive Sub-Carrier Modulation in OFDM Systems	920
Matthias Siebert, Olaf Stauffer, Aachen University, Germany	
5. Coverage Investigations for Adaptive Modulation in 5GHz WLANs	925
Matthias Siebert, Aachen University, Germany;	
Edgar Bolinth, Siemens AG, Germany;	
Olaf Stauffer, Aachen University, Germany;	
Ralf Kern, Siemens AG, Germany	

Session 4G: QoS

1. VoIP in 3G Networks: An End-to-End Quality of Service Analysis	930
Renaud Cuny, Nokia Networks, Finland;	
Ari Lakaniemi, Nokia, Research Center, Finland	
2. A Modeling Framework for Supporting QoS in Mobile Ad-hoc Networks	935
Beongku An, Hongik University, Korea;	
Dohyeon Kim, Cheonan University, Korea;	
Innho Jee, Hongik University, Korea	
3. Performance Evaluation of the QoS Enhanced IEEE 802.11e MAC layer	940
Hong Linh Truong, Gianluca Vannuccini, IBM Research, Switzerland	
4. Collaborative QoS Architecture between DiffServ and 802.11e Wireless LAN	945
Seyong Park, Kyungtae Kim, Doug C. Kim, State University of New York at Stony Brook, USA;	
Sunghyun Choi, Seoul National University, Korea;	
Sangjin Hong, State University of New York at Stony Brook, USA	
5. Joint Connection Level, Packet Level and Link Layer Resource Allocation in Mobile Cellular Networks with QoS Constraints	950
Tung Chong Wong, Institute for InfoComm Research, Singapore;	
Jon W. Mark, University of Waterloo, Canada;	
Kee Chaing Chua, National University of Singapore/Siemens, Singapore;	
Yong Huat Chew, Institute for InfoComm Research, Singapore	

Session 4H: WLAN/Ad Hoc Network 4—Application

1. Performance Behavior of Unmanned Vehicle Aided Mobile Backbone Based Wireless Ad Hoc Networks	955
Izhak Rubin, Runhe Zhang, University of California, USA	
2. Performance of UTRA TDD Ad Hoc and IEEE 802.11b in Vehicular Environments	960
Andre Ebner, Hermann Rohling, Lars Wischhof, Technical University of Hamburg-Harburg, Germany;	
Rudiger Halfmann, Matthias Lott, Siemens AG, Germany	
3. Efficient Discovery of Internet Gateways in Future Vehicular Communication Systems	965
Marc Bechler, Lars Wolf, Technical University of Brunswick, Germany;	
Oliver Storz, Lancaster University, UK;	
Walter Franz, DaimlerChrysler AG, Germany	
4. Multi AP Strategies for SCO Traffic in a Bluetooth based Wireless LAN	970
Anders Dahlberg, Markus Fiedler, Blekinge Institute of Technology, Australia;	
Hans J. Zepernick, Australian Telecommunications CRC, Australia;	
Guven Mercankosk, the University of Western Australia	
5. A New Routing Protocol for Village Radio Network	975
Jing Cheng, Winston K G Seah, National University of Singapore, Singapore	

Poster Session 4: MIMO & Antenna (Smart Antenna)

1. An MIMO-OFDM Technique for High-Speed Mobile Channels	980
Kyung Won Park, Eun Sun Choi, Chung-Ang University, Korea;	
Kyung Hi Chang, ETRI, Korea;	
Yong Soo Cho, Chung-Ang University, Korea	
2. Soft Decision-Based Iterative Interference Cancellation (IIC) in Group-Wise STBC (G-STBC) MIMO Systems	984
Sumei Sun, T. T. Tjhung, Patrick H.W. Fung, Institute for Infocomm Research, Singapore	
3. Simplified Weights Update Algorithm for Semi-Adaptive Ordered Successive Detection in MIMO Wireless Systems	989
Anass Benjebbour, Susumu Yoshida, Kyoto University, Japan	
4. Semi-Blind Identification of Wideband MIMO Channels via Stochastic Sampling	994
Christophe Andrieu, Robert J. Piechocki, Joe P. McGeehan, Simon Armour, University of Bristol, UK	
5. A New Joint Transmit and Receive Optimization Scheme for OFDM-Based MIMO Systems	998
Nadia Khaled, IMEC, Belgium;	
Steven Thoen, Resonext Communications, Belgium;	
Matteo Vizzardi, Claude Desset, IMEC, Belgium	
6. A Novel Smart Antennas Algorithm for 1xEV-DV Systems	1003
Chen Zeqiang, Yang Dacheng, Beijing University of Posts and Telecommunications, China	
7. On Power Reduction Strategies for the Multi-User Downlink with Decentralized Receivers	1007
Thomas Haustein, Martin Schubert, Holger Boche, Heinrich-Hertz-Institut, Germany	

8. Tapered Type PIFA Design for Mobile Phones at 1800 MHz	1012
Byung Chan Kim, Ju Derk Park, Hyung Do Choi, Electronics and Communications Research Institute, Korea	
9. An Adaptive Antenna Array for Single Carrier Modulation System with Cyclic Prefix	1015
Kazunori Hayashi, Taku Kojima, Hideaki Sakai, Kyoto University, Japan	
10. Performance of a Base Station Feedback-Type Adaptive Array Antenna with Mobile Station Diversity Reception	1020
Jeongkeun Choi, Kyushu University, Japan;	
Makoto Tarohmaru, Kyushu Sanyo University, Japan;	
Yoshihiko Akaiwa, Kyushu University, Japan	
11. A New Adaptive Algorithm for MSNR Beamforming in WCDMA System	1025
Fakhru1 Alam, North South University, Bangladesh;	
Donghee Shim, LG Electronics Inc., Korea;	
Brian D. Woerner, Virginia Polytechnic Institute and State University, USA	
12. A New Calibration Algorithm for Smart Antenna Arrays	1030
Andreas Kortke, Technical University of Berlin, Germany	
13. Performance of Dual Antenna Diversity Reception in WCDMA Terminals	1035
Mika Ventola, Esa Tuomaala, Pekka A. Ranta, Nokia Research Center, Finland	
14. Experiments on DOA-Estimation and Beamforming for 60 GHz Smart Antennas	1041
M.S. Choi, G. Grosskopf, D. Rohde, B. Kuhlow, G. Przyrembel, H. Ehlers, Heinrich-Hertz-Institut, Germany	

Session 5A: Propagation/Channel Modeling 5

1. A Comparison between Different Approaches for Fading Evaluation in Wideband Mobile Communications	1046
Filipe D. Cardoso, Polytechnical Institute of Setubal, Portugal;	
Luis M. Correia, Technical University of Lisbon, Portugal	
2. A Blockage based Channel Model for High Altitude Platform Communications	1051
Song Liu, Zhisheng Niu, Youshou Wu, Tsinghua University, China	
3. Maximum Likelihood Channel Parameter Estimation from Multidimensional Channel Sounding Measurements	1056
Andreas Richter, Markus Landmann, Reiner S. Thoma, Ilmenau University of Technology, Germany	
4. Minimax Approximation to Lognormal Sum Distributions	1061
Norman C. Beaulieu, Qiong Xie, University of Alberta, Canada	
5. Effect of Radio Bandwidth on Multipath Clustering	1066
Wei-Ju Chang, Jenn-Hwan Tarn, National Chiao-Tung University, Taiwan	

Session 5B: MIMO 5

1. Adaptive Space-Time Transmit Diversity for MIMO Systems	1070
J. Henry Horng, Ling Li, Jinyun Zhang, Mitsubishi Electric Research Laboratories, USA	
2. Adaptive Modulation for MIMO Systems with V-BLAST Detection	1074
Young-Doo Kim, Inhyoung Kim, Jihoon Choi, Korea Advanced Institute of Science and Technology, Korea;	
Jae-Young Ahn, Electronics and Telecommunications Research Institute, Korea;	
Yong H. Lee, Korea Advanced Institute of Science and Technology, Korea	
3. High Throughput Downlink Cellular Packet Data Access with Multiple Antennas and Multiuser Diversity	1079
David J. Mazzarese, Witold A. Krzymien, University of Alberta, Canada	
4. MIMO-OFDM Channel Estimation Based on Subspace Tracking	1084
Jianxuan Du, Ye (Geoffrey) Li, Georgia Institute of Technology, USA	
5. An Efficient MIMO Receiver Structure for Coded Signals	1089
Ebrahim karami, Mohsen Shiva, University of Tehran, Iran;	
Mohsen Khansari, Iran Telecommunication Research Center, Iran	

Session 5C: Space Time Coding 5

1. Interleave-Division-Multiplexing Space-Time Codes	1094
W.K. Leung, K.Y. Wu, Li Ping, City University of Hong Kong, Hong Kong	
2. Turbo Multiuser Receiver for Space-Time Turbo Coded Downlink CDMA	1099
Jia Shen, Alister G. Burr, University of York, UK	
3. Improved Differential Unitary Space-Time Codes with Multiple Amplitude Modulation	1104
Zheng Du, Jinkang Zhu, University of Science and Technology of China, China	
4. Fully-Diverse Unitary Subgroups Space-Time Codes	1109

Tatsumi Konishi, Aichi Institute of Technology, Japan

5. New Design Criteria of Space-Time Codes for Frequency-Selective Multipath Wireless Channels 1114
Ching-Shyang Maa, Yeong-Cheng Wang, Jiunn-Tsair Chen, National Tsing Hua University, Taiwan

Session 5D: Antenna (Smart Antenna) 5

1. A New High Power Efficient Bit-Interleaved Concatenated STBC 1119
Lu Zhao, Johannes Huber, University Erlangen-Nuernberg, Germany
2. Experiments on the Element Spacing in Multi-Antenna Systems 1124
Volker Jungnickel, Volker Pohl, Clemens von Helmolt, Heinrich-Hertz-Institut, Germany
3. Space-Time Coded Adaptive Transmit Antenna Arrays for OFDM Wireless Systems Utilizing Channel Side Information 1127
Ya-Han Pan, Tsinghua University, China;
Khaled Ben Letaief, Hong Kong University of Science and Technology, Hong Kong;
Zhigang Cao, Tsinghua University, China
4. Comparison of On-line RF Circuitry Calibration Methods for Adaptive Antenna Array Beam Forming Transmitter in Forward Link 1132
Hidekazu Taoka, Takashi Kataoka, Kenichi Higuchi, Taisuke Ihara, Mamoru Sawahashi, NTT DoCoMo Inc., Japan
5. Influence of Channel Characteristics on the Performance of VAA with Deployed STBCs 1138
Andreas Kastrisios, Mischa Dohler, Hamid Aghvami, King's College London, UK

Session 5E: CDMA System 5

1. W-CDMA Downlink Performance Degradation due to Multipath Interference and Channel Estimation Error 1143
Yiannis Socratous, Mischa Dohler, Hamid Aghvami, Centre for Telecommunications Research, UK
2. Upper Bounds on the Access Code Efficiency for CDMA Using Signals with an Interference Free Window 1148
Xiangming Li, M.R. Soleymani, Yingzi Gao, Concordia University, Canada
3. Analytic Approximation of the Effective Bandwidth for Best-Effort Services in UMTS Networks 1153
Dirk Staehle, Kenji Leibnitz, Klaus Heck, Phuoc Tran-Gia, University of Wuzburg, Germany;
Bernd Schroder, Albert Weller, T-Mobile International, Germany
4. Tier-Selection Algorithm with Multi-Class Traffic in CDMA Hierarchical Cellular System 1158
Li-Chun Wang, ChingYu Liao, Yi-Liang Lin, Chung-Ju Chang, National Chiao Tung University, Taiwan
5. Performance of CDMA2000 1xEV-DV System 1163
Lin Ma, Zhigang Rong, R. Thomas Derryberry, Nokia Research Center, USA

Session 5F: OFDM 5 — Coded OFDM/Peak Reduction

1. Performance Degradation of Coded-OFDM due to Phase Noise 1168
Denis Petrovic, Wolfgang Rave, Gerhard Fettweis, Dresden University of Technology, Germany
2. Improved Transmit Diversity Block Coded OFDM Systems for Highly Dispersive Channels 1173
Bing-Hung Chiang, National Taiwan University, Taiwan;
Ding-Bing Lin, National Taipei University of Technology, Taiwan;
Hsueh-Jyh Li, National Taiwan University, Taiwan;
Jia-Li Wang, National Taipei University of Technology, Taiwan
3. LDPC Coded Modulation MIMO OFDM Transciever: Performance Comparison with MAP Eqaulization 1178
Heung-no Lee, University of Pittsburgh, USA
4. Sub-Optimum Peak Reduction Carriers for OFDM Systems 1183
Chong Eng Tan, Ian J. Wassell, University of Cambridge, UK
5. Peak-to-Average Power Ratio Reduction for OFDM Modems 1188
J. Akhtman, B.Z. Bobrovsky, L. Hanzo, University of Southampton, UK

Session 5G: Call Admission Control

1. On the Estimation of User Mobility for Improved Admission Control Algorithms in WCDMA Systems 1193
Leonardo Badia, Michele Zorzi, Samuele Fini, Universita di Ferrara, Italy
2. Uplink Load Estimates in WCDMA with Different Availability of Measurements 1198
Erik Geijer Lundin, Fredrik Gunnarsson, Fredrik Gustafsson, Linkopings Universitet, Sweden
3. On Downlink Admission Control with Fixed Multi-Beam Antennas for WCDMA System 1203
Afif Osseiran, Marten Ericson, Ericsson Research, Sweden

4. A Novel Call Admission Control Scheme for Multimedia CDMA Networks with Power Multiplexing and Imperfect Power Control Tao Shu, Zhisheng Niu, Tsinghua University, China	1208
5. A Framework for Call Admission Control with Threshold Setup and Evaluation of the Performance in WCDMA Systems Leonardo Badia, Michele Zorzi, Universita di Ferrara, Italy	1213

Session 5H: WLAN/Ad Hoc Network 5 — Multicast TCP

1. Reliable Wireless Multicast Using Fast Low-Density Erasure Codes Jin-hwan Chung, Sung-eun Kim, John Copeland, Georgia Institute of Technology, USA	1218
2. Performance Analysis of Multicast Transmission in WLAN Matthias Lott, Siemens AG, Germany; Alexey Sitalov, Evgeny Linsky, St. Petersburg State University of Aerospace Instrumentation, Russia; Hui Li, Siemens AG, Germany	1223
3. Cache Data Access System in Ad-Hoc Networks Takaaki Moriya, Hitoshi Aida, University of Tokyo, Japan	1228
4. Analysis of Packet Transmission for Ad-hoc Mobile Wireless Networks Yumiko Tateishi, Kazuhiko Fukawa, Hiroshi Suzuki, Tokyo Institute of Technology, Japan	1233
5. A Multicast Protocol for Physically Hierarchical Ad Hoc Networks Young-Bae Ko, Ajou University, Korea; Sung-Ju Lee, Hewlett-Packard Labs, USA; Kang-Yong Lee, Ajou University, Korea	1238

Poster Session 5: OFDM System/MC-CDMA System & AMC

1. PAPR Reduction of OFDM Systems Using Input Sequence Envelope Scaling P. Foomooljareon, W.A.C. Fernando, K.M. Ahmed, Asian Institute of Technology, Thailand	1243
2. Time-Frequency Spread OFDM/FHMA Kiyoshi Hamaguchi, Communications Research Laboratory, Japan; Lajos Hanzo, University of Southampton, UK	1248
3. A Frequency Scheduling Method Using Antenna Diversity for MC-CDM System Shigehiko Tsumura, Shinsuke Hara, Osaka University, Japan	1253
4. Performance of Multicarrier CS/CDMA in Frequency-Selective Rayleigh Fading Channels Kwan Woong Ryu, Jin Ok Park, Yong Wan Park, Yeungnam University, Korea	1258
5. A Study on the PAR Reduction by Hybrid Algorithm Based on the PTS and SLM Techniques Pavel A. Pushkarev, Kwan-Woong Ryu, Kook-Yeol Yoo, Yong-Wan Park, Yeungnam University, Korea	1263
6. A Novel Two-Layered Suboptimal Approach to Partial Transmit Sequences Wong Sai Ho, AS Madhukumar, Francois Chin, Institute for Infocomm Research, Singapore	1268
7. Space-Time-Frequency Processing for OFDM Wireless Mobile Communications Byung-Chul Kim, Samsung Electronics Co. Ltd., Korea; I-Tai Lu, Polytechnic University, USA	1273
8. On the Error Probability Performance of Non-Linearly Distorted OFDM Signals M.R.D. Rodrigues, University of Cambridge, UK; J.E. Mitchell, I. Darwazeh, University College London, UK	1278
9. Pilot Power Allocation for OFDM Systems Jiming Chen, Youxi Tang, Shaoqian Li, University of Electronic Science and Technology of China, China	1283
10. Some Issues of Complexity and Training Symbol Design for OFDM Frequency Offset Estimation Methods Based on BLUE Principle Hlaing Minn, University of Texas at Dallas, USA; Poramate Tarasak, Vijay K. Bhargava, University of Victoria, Canada	1288
11. Convolutional Coded Pulse-Position Modulation on Wireless Optical Communication Hyuncheol Park, Information and Communications University, Korea	1293
12. Performance Evaluation for Integrated Voice/Data Wireless Networks with Link Adaptation Jean-Lien C. Wu, Hung-Huan Liu, National Taiwan University of Science and Technology, Taiwan	1298

Session 6A: Equalization/Channel Estimation 1

1. On Channel Estimation for OFDM Systems in Multipath Environments with Relatively Large Delay Spread Wookwon Lee, University of Arkansas, USA	1303
---	------

2. Improved Channel Estimation Using Noise Reduction for OFDM Systems	1308
H. Zamiri-Jafarian, M.J. Omidi, S. Pasupathy, University of Toronto, Canada	
3. Iterative Channel Estimator and Equalizer for OFDM Modulation Systems	1313
Ping He, Kai-Uwe Schmidt, Chin Keong Ho, Sumei Sun, Institute for Communications Research, Singapore	
4. Time-Domain Method for Tracking Dispersive Channels in OFDM Systems	1318
Timo Roman, Mihai Enescu, Visa Koivunen, Helsinki Univ. of Technology, Finland	
5. Pilot Symbol Initiated Iterative Channel Estimation and Decoding for QAM Modulated OFDM Signals	1322
Jong-Ho Lee, Yong-Hwa Kim, Seong-Cheol Kim, Seoul National University, Korea;	
Jae Choong Han, Myong Ji University, Korea;	

Session 6B: Transceiver Architecture 1 — Transmitter

1. Proposal of Transmission Architecture for Mobile Terminals Employing EER Power Amplifier	1327
May Suzuki, Taizo Yamawaki, Tomonori Tanoue, Yasuyuki Ookuma, Ryosuke Fujiwara, Satoshi Tanaka, Hitachi, Ltd., Japan	
2. An Adaptive Power Amplifier Lineariser Based on a Multilayer Perceptron	1331
N. Naskas, Y. Papananos, National Technical University of Athens, Greece	
3. An Improved Digital-IF Transmitter Architecture for Highly-Integrated W-CDMA Mobile Terminals	1335
Vincent W. Leung, Lawrence E. Larson, University of California, USA;	
Prasad Gudem, Qualcomm Inc., USA	
4. Optimization of Link Adaptation with a Practical Power Consumption Model	1340
Fei Tang, Claude Dessel, Marc Moonen, Hugo De Man, IMEC, Belgium	
5. Joint Polynomial and Look-Up-Table Power Amplifier Linearization Scheme	1345
Hsing-Hung Chen, Ching-Shyang Maa, Yeong-Cheng Wang, Jiunn-Tsair Chen, National Tsing Hua University, Taiwan	

Session 6C: Space Time Coding 6

1. Decoding Order Schemes for the Layered Receiver of Multiple Space-Time Codes On the Fast Flat Fading Channel	1350
Eun Jeong Yim, Young Min Ki, Dong-Ku Kim, Yonsei University, Korea	
2. Wireless Communication Based on LDPC and Adaptive Space-Time Coded MQAM	1354
Jie Yang, Wuhan University of Technology, China;	
Moon Ho Lee, Chonbuk National University, Korea;	
Guo Zhen Tan, Wuhan University of Technology, China	
3. Improved Design Criteria and New Codes for Space-Frequency Trellis Coding with Interleaver over Frequency Selective Fading Channels	1358
Yukihiro Sasazaki, Tomoaki Ohtsuki, Tokyo University of Science, Japan	
4. Artificial Delay Added Space Time Turbo Coding on OFDM in Correlated Fading Channel	1363
Kenichi Miyoshi, Mitsuru Uesugi, Osamu Kato, Panasonic Mobile Communications Co., Ltd., Japan;	
Atsushi Matsumoto, Panasonic Mobile Communications Kanazawa R&D Lab. Co., Ltd., Japan	
5. Space-Time Block Coded IQ-Interleaved Joint Coding and Modulation for AWGN and Rayleigh Fading Channels ...	1367
S.X. Ng, Lajos Hanzo, University of Southampton, UK	

Session 6D: Satellite System

1. Timeslot Assignment for an Interactive Satellite Multimedia Network with Multiclass RCSTs and Services	1372
Ki-Dong Lee, ETRI, Korea;	
Kun-Nyeong Chang, Silla University, Korea;	
Ho-Jin Lee, ETRI, Korea	
2. An Analysis of the Impact of Earth Rotation on LEO Satellite Mobility Models	1376
Boon Sain Yeo, National University of Singapore, Singapore	
3. Performance Evaluation of SIP-Based Session Establishment over Satellite-UMTS	1381
Victor Y.H. Kueh, Rahim Tafazolli, Barry Evans, University of Surrey, UK	
4. A Simulation-Based Handoff Approach for LEO Satellite Networks	1386
B. S. Yeo, Institute for Communications Research, Singapore;	
L.F. Turner, Imperial College of Science, Technology and Medicine, Singapore	
5. A Distributed Delay-Constrained Multicast Tree Algorithm in LEO Satellite Networks	1391
Wang Liang, Zhang Nai-tong, Harbin Institute of Technology, China	

Session 6E: CDMA System 6

1. Pre-Rake Assisted Rake Receiver for TDD WCDMA System	1396
Suk-Hyen Jung, Nak-Myeong Kim, Hee-Jung Suh, Ewha Womans University, Korea	
2. UTRA TDD Dynamic Channel Allocation in Uplink with Slow Reallocation	1401
Otto Lehtinen, Nokia Research Center, USA; Janne Kurjeniemi, University of Jyvaskyla, Finland	
3. Resource Metric Mapping Function for a TDD-CDMA System Supporting WWW Traffic	1406
Yeonwoo Lee, Steve McLaughlin, University of Edinburgh, UK; Dong Keun Jeon, Incheon City College, Korea	
4. Time Slot Allocation Based on a Path Gain Division Scheme for TD-CDMA TDD Systems	1410
Jad Nasreddine, Xavier lagrange, ENST Bretagne, France	
5. Fast Permutation Based Time Slot Allocation for 3G WCDMA TDD Systems	1415
Guodong Zhang, Eldad Zeira, InterDigital Communications Corp., USA	

Session 6F: OFDM 6

1. Capacity of Ultra-Wideband OFDM	1420
Rahul Gupta, Ahmed H. Tewfik, University of Minnesota, USA	
2. Generating UWB-OFDM Signal Using Sigma-Delta Modulator	1425
Ebrahim Saberinia, Ahmed H. Tewfik, University of Minnesota, USA	
3. Filtered OFDM/OQAM Transmission System	1430
Mohamad Aoude, Robert A. Vallet, ENST, France	
4. On the Effects of User Mobility on the Uplink of an OFDMA System	1433
Dirk Galda, Hermann Rohling, Technical University Hamburg-Harburg, Germany; Elena Costa, Siemens AG, Germany	
5. SS-OFDM-F/TA System Packet Size and Structure for High Mobility Cellular Environments	1438
Robert Novak, Witold A. Krzymien, University of Alberta/TRLabs, Canada	

Session 6G: Packet Scheduling 1

1. Adaptive Rate Control Scheme for Handoff and Its Performance Evaluation in Mobile Multimedia Networks	1445
Sung-Eun Kim, Georgia Institute of Technology, USA; Heechang Kim, Telcordia Technology Inc., USA; John A. Copeland, Georgia Institute of Technology, USA	
2. Scheduling Methods with Transmit Power Constraint for CDMA Packet Services	1450
Jung-Ho Yoon, Min-Joung Sheen, Sin-Chong Park, Information and Communications University, Korea	
3. Network Performance of Transmit and Receive Antenna Diversity in HSDPA under Different Packet Scheduling Strategies	1454
Juan Ramiro-Moreno, Aalborg University, Denmark; Klaus I. Pedersen, Preben E. Mogensen, Nokia Networks, Denmark	
4. Dynamic Packet Scheduling for Wireless Channel with Varying Capacity	1459
Liang Zhang, Tony T. Lee, The Chinese University of Hong Kong, Hong Kong	
5. Interaction between Fast Scheduling Diversity and Rake Receivers	1464
Neelesh B. Mehta, Broadcom, USA; Zoran A. Kostic, Thomson Multimedia, USA; Moe Z. Win, MIT, USA	

Session 6H: WLAN/Ad Hoc Network 6—MAC

1. An Adaptive RTS/CTS Control Mechanism for IEEE 802.11 MAC Protocol	1469
Huei-jui Ju, Izak Rubin, Yen-Cheng Kuan, University of California, USA	
2. Field Trial Results at DLC Layer of a HiperLAN/2 Prototype	1474
Romain Rollet, Corinne Rosier, Herve Bonneville, Christophe Mangin, Mitsubishi Electric ITE-TCL, France	
3. Performance of IEEE 802.11b Wireless LAN in an Emulated Mobile Channel	1479
Christopher Steger, Predrag Radosavljevic, J. Patrick Frantz, Rice University, USA	
4. Energy-Efficient Interference Avoidance for Interconnected Bluetooth Personal Area Networks	1484
Petar Popovski, Liljana Gavrilovska, Thibault Renier, Hanane Fathi, Ramjee Prasad, Aalborg University, Denmark	
5. Performance of Physical (PHY) and Medium Access Control (MAC) Layers of IEEE 802.11b in the Presence of Bluetooth Piconets	1489
Wang Feng, A. Nallanathan, Garg Hari Krishna, National University of Singapore, Singapore	

Volume 3

Poster Session 6: Wireless Networks & WLAN

1. Mobility Management in All-IP Two-Tier Cellular Networks	1493
Bor-Jiunn Hwang, Van Nung Institute of Technology, Taiwan; Jung-Shyr Wu, National Central University, Taiwan; Wang-Hsing Hsu, Van Nung Institute of Technology, Taiwan	
2. Agent Support for PSE Migration in VHE	1497
Yu Yuhai, Zhang Ping, Beijing University of Posts and Telecommunications, China	
3. An Adaptive Hierarchical Mobile IPv6 with Route Optimization	1502
Seung-Hee Hwang, Korea University, Korea; Bo-Kyong Lee, Korea Polytechnic University, Korea; Youn-Hee Han, Samsung AIT, Korea; Chong-Sun Hwang, Korea University, Korea	
4. Concatenated Wireless Roaming Security Association and Authentication Protocol Using ID-Based Cryptography	1507
Byung-Gil Lee, Hyun-Gon Kim, Sung-Won Sohn, ETRI, Korea; Kil-Houn Park, Kyungpook National University, Korea	
5. Generic System Architecture for 4G Mobile Communications	1512
Vangelis Gazis, Nikos Housos, Athanassia Alonistioti, Lazaros Merakos, University of Athens, Greece	
6. A Fuzzy-Based Dynamic Channel Borrowing Scheme for Wireless Cellular Networks	1517
Yao-Tien Wang, National Central University, Taiwan	
7. An Enhancement Scheme for TCP over Mobile Ad hoc Networks	1522
Jin-Hee Choi, See-Hwan Yoo, Chuck Yoo, Korea University, Korea	
8. Mobile Cluster based Call Admission Control in Wireless Mobile Networks	1527
Jeong-Jae Won, Eui-Seok Hwang, Hyong-Woo Lee, Choong-Ho Cho, Korea University, Korea	
9. Transmission Control for Wireless Networks with Inaccurate Channel Conditions: A Game-Theoretic Approach	1532
Xiang Duan, Zhisheng Niu, Junli Zheng, Tsinghua University, China	
10. Applications of Delegation Schemes for Securing Future Reconfigurable Terminals	1536
Chan Yeob Yeun, Georgios Kalogridis, Gary Clemo, Toshiba Telecommunications Research Laboratory, England	
11. Evaluation of Wireless System with Connection/Connectionless Mixed Multicast Protocol in Spatially Correlated Mobile Radio Channel	1541
Atsushi Takahashi, Takeshi Hattori, Sophia University, Japan	
12. Efficient Radio Network Optimization	1546
Yun Sik Kim, Hyun-Meen Jung, KT, Korea	
13. Determination of Fragmentation Size in Wireless System	1550
Yeong-Hyeon Kwon, Dong-Jo Park, Sang-Min Lee, Mi-Kyung Oh, Korea Advanced Institute of Science and Technology, Korea	
14. A Unit with Functions of Spectrum Monitoring, Self-Excitation Detection and Isolation Degree Test for Wireless Relay Station	1554
Sujian Zhao, Xin Su, Chu Zhang, Yan Yao, Tsinghua University, China	
15. Receiver-Controlled Joint Source/Channel Coding on the Application Level, for Video Streaming over WLANs	1558
Patrik Österberg, Daniel Forsgren, Tingting Zhang, Mid-Sweden University, Sweden	
16. Non-Uniform Polling Scheme with Activity Detection for Real-Time Services in Wireless LAN	1562
Won Soo Kim, Samsung Advanced Institute of Technology, Korea; Jeongsim Kim, Korea University, Korea; Seung Eun Hong, ETRI, Korea; Chung Gu Kang, Korea University, Korea	
17. Flexible Linearity Profile Low Noise Feedforward Amplifiers for Improving Channel Capacity	1567
G.T. Watkins, P.A. Warr, University of Bristol, UK	
18. Load Threshold for Connection State Scheme Supporting Packet Data Service in Wireless Networks	1571
Cheon Won Choi, Woo Cheol Shin, Jin Kyung Park, Dong Joon Kim, Jea Hwan Ju, Dankook University, Korea	

Session 7A: Equalization/Channel Estimation 2

1. Adaptive Prediction Iterative Channel Estimation for OFDM Signal Reception in a Frequency Selective Fading Channel	1576
Shinsuke Takaoka, Fumiaki Adachi, Tohoku University, Japan	
2. Pilot-Aided Channel Estimation for OFDM/OQAM	1581
Jean-Philippe Javaudin, Dominique Lacroix, France Telecom R&D, France; Alexandre Rouxel, Wavecom, France	
3. Threshold Channel Estimation for OFDM in Wireless Systems	1586
Yan Wang, Chi-Ying Tsui, Roger S. Cheng, Wai Ho Mow, Hong Kong University of Science and Technology, Hong Kong	
4. Design of Implementation-Efficient Channel Estimation Filter for Wireless OFDM Transmission	1590
Jae-Ho Ryu, Yong-Hwan Lee, Seoul National University, Korea	
5. An Improved 2-Dimensional Pilot-Symbols Assisted Channel Estimation in OFDM Systems	1595
Zhang Jianhua, Zhang Ping, Beijing University of Posts and Telecommunications, China	

Session 7B: Transceiver Architecture 2 — Receiver

1. Self-Orienting Receiver for Indoor Wireless Infrared Links at High Bit Rates	1600
M. Castillo-Vázquez, A. Puerta-Notario, University of Málaga, Spain	
2. Joint Compensation of IQ Imbalance and Phase Noise	1605
Jan Tubbax, Boris Come, Liesbet Van der Perre, Stephane Donnay, Marc Engels, Claude Dessel, IMEC, Belgium	
3. Performance of Iterative Multiuser Receiver for Turbo-Coded DS-CDMA	1610
Huy G. Vu, University of Saskatchewan, Canada; R.M.A.P. Rajatheva, University of Moratuwa, Sri Lanka; W.A.C. Fernando, Asian Institute of Technology, Thailand	
4. Design of Simplified Receivers for Space-Time Bit-Interleaved Coded Modulation Systems	1614
Inkyu Lee, Korea University, Korea; Carl-Erik W. Sundberg, SundComm, USA	

Session 7C: Interference Cancellation/MUD 1

1. Matched-Filter Based Iterative Soft Decision Interference Cancellation Employing the Distribution of Interference	1619
Jurgen F. Roessler, Johannes B. Huber, University Erlangen-Nuremberg, Germany	
2. Field Experiments on Multipath Interference Canceller Associated with AMC in HSDPA	1624
Takahiro Asai, Kenichi Higuchi, Mamoru Sawahashi, NTT DoCoMo Inc, Japan	
3. Iterative Soft Sequential Estimation Aided Differential Acquisition of m-Sequences	1629
Lie-Liang Yang, Lajos Hanzo, University of Southampton, UK	
4. Performance Analysis of Simple Transversal-filter-based Multipath Interference Canceller with Analytically Derived Tap Coefficients for Reverse Link of Multicarrier DS-CDMA Systems	1634
Yoshihiko Asano, Fujitsu Laboratories Ltd., Japan; Yoshimasa Daido, Kanazawa Institute of Technology, Japan	
5. Cancellation Accuracy in CDMA Pilot Interference Cancellation	1639
Shimon Moshavi, Daniel Yellin, Yoni Perets, John S. Sadowsky, Intel Corporation, Israel	

Session 7D: UWB

1. Performance of UWB Time-Hopping Spread-Spectrum Impulse Radio in Multipath Environments	1644
Guangrong Yue, Shaoqian Li, University of Electronic Science and Technology of China, China; Lijia Ge, Chongqing Sinotel Digital Communications and Signal Processing Institute, China	
2. Spectrum Control by Means of the TH Code in UWB systems	1649
Lorenzo Piazza, University "La Sapienza," Italy; Jac Romme, IMST GmbH, Germany	
3. On the Performance of Bi-Phase Modulated UWB Signals in a Multipath Channel	1654
Woo Cheol Chung, Dong Sam Ha, Virginia Tech, USA	
4. Time-Space Path Model in Wide-Band Mobile Communications	1659
Hideki Omote, Teruya Fujii, Japan Telecom Co., Ltd., Japan	
5. A New UWB Pulse Generator for FCC Spectral Masks	1664
A. B. Parr, University of California, USA; B.L. Cho, Sunchon National University, Korea; Z. Ding, University of California, USA	

Session 7E: CDMA System 7

1. Joint PN Code Acquisition and DOA Estimation in Asynchronous DS-CDMA Systems	1667
Chiao-Yao Chuang, Xiaoli Yu, C. -C. Jay Kuo, University of Southern California, USA	
2. Sequence Selection Scheme in DS-CDMA Systems	1672
Ho Yuet Kwan, Tat Ming Lok, the Chinese University of Hong Kong, Hong Kong	
3. Joint Detection for On/Off Uplink Traffic in the TD-SCDMA System	1677
Ji Young Yun, Dan Keun Sung, KAIST, Korea	
4. A Study on Synchronization of Hybrid TDMA/Binary CDMA	1681
Ho Seong Ahn, CASUH Corp., Korea;	
Sung Woong Ra, Chungnam University, Korea	
5. A Design of High Speed Multi-Path Searcher Using Dual Scrambling Code Generators for WCDMA	1685
Daeho Kim, YounOk Park, ETRI, Korea;	
Whan Woo Kim, Chungnam National University, Korea	

Session 7F: Packet Scheduling 2

1. Downlink Intercell Coordination for DS-CDMA Non Real Time Data	1689
Sung-Hyuk Kwon, Seong-Lyun Kim, Information and Communications University, Korea;	
Riku Jantti, University of Vaasa, Finland	
2. Packet Scheduling for MIMO Cellular Systems	1694
Oh-Soon Shin, Kwang Bok (Ed) Lee, Seoul National University, Korea	
3. On Minimum Time Span Scheduling of Non-Real-Time Data in Uplink of DS-CDMA Systems	1699
Riku Jantti, University of Vaasa, Finland	
Deze Zhao, Helsinki University of Technology, Finland	
4. User Satisfaction Models and Scheduling Algorithms for Packet-Switched Services in UMTS	1704
Nicolas Enderle, Bouygues Telecom R&D, France;	
Xavier Lagrange, ENST Bretagne, France	
5. Schedulers for 1xEV-DO: Third Generation Wireless High-Speed Data Systems	1710
ChingYao Huang, HueiYuan Su, National Chiao Tung University, Taiwan;	
Stan Vitebsky, Pi-Chun Chen, Lucent technologies, USA	

Session 7G: Wireless Networks 1 — TCP

1. TCP Performances over Wireless Link Deploying Delayed ACK	1715
W. Lilakiatsakun, Mahanakorn University of Technology, Thailand;	
A. Seneviratne, University of New South Wales, Australia	
2. New Flow Control Schemes of TCP for Multimodal Mobile Hosts	1720
Kazuya Tsukamoto, Yutaka Fukuda, Yoshiaki Hori, Yuji Oie, Kyushu Institute of Technology, Japan	
3. Wireless TCP Model for Short-Lived Flows	1725
Sangheon Pack, Sungyong Ahn, Yanghee Choi, Seoul National University, Korea;	
Seungmo Choe, KT, Korea	
4. A New Method to Improve the Performance of TCP SACK over Wireless Links	1730
Jeng-Ji Huang, National Taiwan University, Taiwan;	
Jin-Fu Chang, National Chi Nan University, Taiwan	
5. Improving TCP Performance in Heterogeneous Mobile Networks	1735
Chang-Jung Kao, Wanjiun Liao, Chin-Hei Chien, National Taiwan University, Taiwan;	
Jen-Chi Liu, ITRI, Taiwan	

Session 7H: WLAN/Ad Hoc Network 7 — Routing

1. A Neighbor-Table-Based Multipath Routing in Ad Hoc Networks	1739
Zhongbang Yao, Junfeng Jiang, Pingyi Fan, Zhigang Cao, Tsinghua University, China;	
Victor O. K. Li, University of Hong Kong, Hong Kong	
2. DL-GRID: A QoS Routing Protocol for Ad Hoc Networks	1744
Huey-Ing Liu, Yi-Yung Li, Fu-Jen Catholic University, Taiwan	
3. Multi-Rate Aware Routing Protocol for Mobile Ad Hoc Networks	1749
Yongho Seok, Jaewoo Park, Yanghee Choi, Seoul National University, Korea	
4. Load-Aware On-Demand Routing (LAOR) Protocol for Mobile Ad hoc Networks	1753
Joo-Han Song, Vincent Wong, Victor C.M. Leung, University of British Columbia, Canada	

5. Lower Bound on Path Availability in Ad Hoc Network	1758
Dan Yu, Hui Li, Siemens AG, Germany	

Poster Session 7: WLAN/Ad Hoc Network & Location Management

1. Service Discovery based on Multicast DNS in IPv6 Mobile Ad-hoc Networks	1763
Jaehoon Jeong, Jungsoo Park, Hyoungjun Kim, ETRI, Korea	
2. A Novel Multiple Access Protocol for Mobile Ad Hoc Networks with Smart Antennas	1768
Jun Yang, Jiandong Li, Xidian University, China	
3. A Study on Protocol, Implementation and Throughput Evaluation for Multihop Wireless LAN	1773
Yasunori Owada, Kenichi Mase, Niigata University, Japan	
4. Performance Evaluation of MIR (Mobile IP Reservation Protocol), Based on Stochastic Automata Networks	1778
L. Mokdad, Université de Paris Dauphine, France;	
J. Ben Othman, Université de Versailles Saint-Quentin, France	
5. Design Alternatives for IP in Vehicles	1783
Christian Maihofer, DaimlerChrysler Research and Technology, Germany;	
Marc Bechler, Technical University of Braunschweig, Germany	
6. Analysis and Simulation of Fast-OLSR	1788
Mounir Benzaid, Pascale Minet, Khaldoun Al Agha, INRIA, France	
7. A Multiple Access Collision Avoidance Protocol for Multicast Service in Mobile Ad Hoc Networks	1793
Ki-Ho Lee, Dong-Ho Cho, KAIST, Korea	
8. Experiments on Radio Interference between Wireless LAN and Other Radio Devices on a 2.4 GHz ISM Band	1798
Jin-A Park, Seung-Keun Park, Dong-Ho Kim, Pyung-Dong Cho, ETRI, Korea;	
Kyoung-Rok Cho, Chungbuk National University, Korea	
9. Interworking between WLANs and Third-Generation Cellular Data Networks	1802
Apostolis K. Salkintzis, Motorola, Greece	
10. Q-Bridge: A QoS Enabled Bridging Model for 802.11 Access Point	1807
Ming-Chung Tang, Li-Ping Tung, Wei-Kuan Shih, National Tsing-Hua University, Taiwan	
11. Improving the Efficiency and Fairness of Time-Spread Multiple-Access (TSMA) Using Adaptive P-Persistency	1811
Jong-Hoon Youn, University of Nebraska at Omaha, USA;	
Seungjin Park, Michigan Technological University, USA	
12. Ad Hoc Routing for Cellular Coverage Extension	1816
Ingo Gruber, Georg Bandouch, Technische Universität München, Germany;	
Hui Li, Siemens AG, Germany	
13. Routing Security and Data Confidentiality for Mobile Ad hoc Networks	1821
Keng Seng Ng, National University of Singapore, Singapore;	
Winston K. G. Seah, Institute for Infocomm Research, Singapore	
14. INK: Implicit Neighbor Knowledge Routing in Ad Hoc Networks	1826
Joon Yoo, Hong-Ryeol Gil, Chong-Kwon Kim, Seoul National University, Korea	
15. A Decentralized Location-based Channel Access Protocol for Inter-Vehicle Communication	1831
Shamukh Katragadda, Ganesh Murthy CNS, Ranga Rao MS, Mohan Kumar S, DaimlerChrysler Research Centre India Pvt Ltd., India;	
Sachin R, Birla Institute of Science & Technology, India	
16. Importance of Accurate Mobility Modelling in Teletraffic Analysis of the Mobile Environment	1836
D.R. Basgeet, University of Bristol, UK;	
J. Irvine, University of Strathclyde, Scotland;	
A. Munro, M.H. Barton, University of Bristol, UK	

Session 8A: Equalization/Channel Estimation 3

1. Iterative Cyclic Prefix Reconstruction for Coded Single-Carrier Systems with Frequency-Domain Equalization (SC-FDE)	1841
Taewon Hwang, Ye (Geoffrey) Li, Georgia Institute of Technology, USA	
2. Low Complexity Turbo-like Decision Feedback Equalization for Broadband Wireless Single Carrier Systems	1846
A. Koppler, A. Springer, Johannes Kepler University, Austria;	
M. Huemer, University of Applied Sciences, Austria;	
R. Weigel, Friedrich Alexander University, Germany	
3. Adaptive MIMO Decision Feedback Equalization for Receivers in Time-Varying Channels	1851
Jihoon Choi, Korea Advanced Institute of Science and Technology, Korea;	
Heejung Yu, Electronics and Telecommunications Research Institute, Korea;	
Yong H. Lee, Korea Advanced Institute of Science and Technology, Korea	

4. Iterative Channel Equalization for the Multicode DS-CDMA Downlink	1857
Eric Hardouin, Christophe Laot, ENST Bretagne, France	
5. A Novel Blind Adaptive Equalization in Time-Varying Channel with ISI	1862
Mi-Kyung Oh, Dong-Jo Park, Yeong-Hyeon Kwon, Korea Advanced Institute of Science and Technology, Korea	

Session 8B: Modulation and Coding 1 — LDPC

1. LDPC Assisted Block Coded Modulation for Transmission over Rayleigh Fading Channels	1867
F. Guo, S.X. Ng, Lajos Hanzo, University of Southampton, UK	
2. Performance of LDPC Code Based D-BLAST System	1872
Eunok Lee, Jaebum Kim, Hyuncheol Park, Hyuckjae Lee, Information and Communications University, Korea	
3. Block Length of LDPC Codes in Fading Channels	1876
Wei Wu, Sangjin Hong, Do-sik Yoo, State University of New York at Stony Brook, USA;	
4. Performance of Low-Density Parity-Check (LDPC) Code with UMP BP-Based Algorithm and Quantizer on Rayleigh Fading Channels	1881
Akinori Ohhashi, Tomoaki Ohtsuki, Tokyo University of Science, Japan	
5. An LDPC-Coded Spatial Multiplexing OFDMA System with Iterative Demodulation and Decoding	1886
Yun Hee Kim, Kwang Soon Kim, Sang Hyun Lee, Kyung Hi Chang, Electronics and Telecommunications Research Institute, Korea	

Session 8C: Interference Cancellation/MUD 2

1. Recursive Vector Viterbi Algorithm for Multibeam Interference Cancellers	1890
Satoshi Denno, DoCoMo Communications Laboratories Europe GmbH, Germany	
2. Parallel Interference Cancellation Receiver Performance in the Presence of TDMA Interference	1895
Jukka Nuutinen, Kari Horneman, Kari Pajukoski, Nokia, Finland	
3. Performance of Parallel Interference Cancellation with Reverse-Link Synchronous Transmission Technique for DS-CDMA System in Multipath Fading Channels with Imperfect Power Control	1900
Seung-Hoon Hwang, Min-Seok Oh, Jin Sung Choi, LG Electronics, Korea;	
Yong-Seok Kim, Keum-Chan Whang, Yonsei University, Korea	
4. Performance of the Multi-stage Variable Group Hybrid Interference Cancellation Scheme with Timing and Phase Errors	1905
Kay Wee Ang, Witold A. Krzymien, University of Alberta, Canada	
5. Multirate SIC Receiver with Several Amplitude Estimation Methods for UMTS FDD Uplink	1910
Isabel Barbancho, Ana M. Barbancho, Lorenzo J. Tardon, J. Tomas Entrambasaguas, ETSI de Telecommunicacion, Spain	

Session 8D: Adaptive Modulation Coding (AMC) 1

1. Proposal of Single Carrier OFDM Technique with Adaptive Modulation Method	1915
Hideo Kobayashi, Mie University, Japan;	
Tadayuki Fukuhara, Hao Yuan, Yoshio Takeuchi, KDDI R&D Laboratories Inc., Japan	
2. Selection of Channel Coding for Low-Power Wireless Systems	1920
Claude Desset, Andrew Fort, IMEC, Belgium	
3. Path-Time Coding for Downlink Multi-User CDMA over Multipath Channels	1925
Chung-Lien Ho, Jwo-Yuh Wu, Ta-Sung Lee, National Chiao Tung University, Taiwan	
4. Space-Time Adaptive Detection in Turbo-Coded DS-CDMA Wireless Systems over Rayleigh Fast-Fading Channels	1930
Walaa Hamouda, Concordia University, Canada;	
Peter McLane, Queen's University, Canada	
5. Determining the Optimum Threshold Values of MCS Levels for Retransmission Packets in HARQ Schemes	1935
Bang Chul Jung, Jae Kyun Kwon, Dan Keun Sung, KAIST, Korea	

Session 8E: CDMA System 8

1. Radio Resource Metric Estimation for Wireless CDMA Communication Systems Maximising Radio Resource Utilisation	1940
Yeonwoo Lee, Stephen McLaughlin, University of Edinburgh, UK;	
Sangboh Yun, Samsung Advanced Institute of Technology, Korea	
2. Spectrum Sharing for Frequency Hopped CDMA Systems with Overlaying Cellular Structures	1945

Li-Chun Wang, Kuan-Jiin Shieh, National Chiao Tung University, Taiwan	
3. A Generalized Processor Sharing Approach to Resource Allocation for QoS in MultiCode-CDMA Networks	1950
Peng-Yong Kong, National University of Singapore, Singapore	
4. On Optimizing FER Target for CDMA2000 Downlink	1955
Sunil Kandukuri, Etienne Chaponnier, Walid Hamdy, Qualcomm Inc., U.S.A.	
5. A Delay NAK Retransmission Scheme Based on Channel State for Mobile Multimedia Communications	1960
Yi Wu, Zhisheng Niu, Junli Zheng, Tsinghua University, China;	
Tamio Saito, Fujitsu Research and Development Center, China	

Session 8F: Handoff — Heterogeneous Systems

1. Impact of Platform Motion on Soft Handover in High Altitude Platform IMT-2000 System	1964
Song Liu, Zhisheng Niu, Youshou Wu, Tsinghua University, China	
2. Design and Evaluation of a Handover Decision Strategy for 4th Generation Mobile Networks	1969
Wenhui Zhang, Juergen Jaehnert, Klaus Dolzer, University of Stuttgart, Germany	
3. Impact of Soft Handoff Threshold and Maximum Active Group Size	
on Base Station Downlink Transmit Power in the UMTS System	1974
Dan Avidor, Lucent Technologies, USA;	
Nidhi Hegde, INRIA Sophia Antipolis, France;	
Sayandev Mukherjee, Lucent Technologies, USA	
4. Performance Evaluation of Soft Handover in a Realistic UMTS Network	1979
Ingo Forkel, Marc Schinnenburg, Aachen University, Germany;	
Bianca Wouters, Vodafone, Netherlands	
5. Buffering Requirements for Lossless Vertical Handoffs in Wireless Overlay Networks	1984
Muhammed Salamat, Fatma Tansu, Nabil Khalil, Eastern Mediterranean University, Turkey	

Session 8G: Wireless Networks 2 — Positioning and Paging

1. Location Based Services for Next Generation Wireless Mobile Networks	1988
Woo-Jin Choi, Sirin Tekinay, New Jersey Institute of Technology, USA	
2. A New Method for Positioning of Mobile Users by Comparing a Time Series of Measured Reception Power Levels with Predictions	1993
Heiko Schmitz, Martin Kuipers, Kurt Majewski, Siemens AG, Germany;	
Peter Stadelmeyer, RISC Software GmbH, Austria	
3. Terminal Register-Based Paging Strategy for Cellular Mobile Networks	1998
Bongsue Suh, Electronics and Telecommunications Research Institute, Korea;	
Jin Seek Choi, Information and Communications University, Korea;	
Song-In Choi, Electronics and Telecommunications Research Institute, Korea	
4. A Neural Network-Based Mobile Positioning with Hierarchical Structure	2003
H. Zamiri-Jafarian, M.M. Mirsalehi, I. Ahadi-Akhlaghi, H. Keshavarz, Ferdowsi University, Canada	
5. SIP-based Architecture of Broadband Wireless Access Systems Inside the GSM/EDGE Network	2008
G. Plitsis, T. Sahin, Aachen University, Germany	

Session 8H: WLAN/Ad Hoc Network 8 — Topics in Multi-hop Wireless Networks (1)

1. A Multi-Protocol Wireless Multi-Hop Network Employing a New Efficient Hybrid Routing Scheme	2013
Minoru Katayama, Kohei Mizuno, Masayoshi Nakayama, Masatoshi Shimizu, NTT Network Innovation Laboratories, Japan	
2. A Distributed Stable Backbone Maintenance Protocol for Ad Hoc Wireless Networks	2018
Izhak Rubin, Xiaolong Huang, Y. C. Liu, Huei-jun Ju, University of California, USA	
3. Bluetooth Enables In-door Mobile Location Services	2023
Saowanee Thongthammachart, Henning Olesen, Technical University of Denmark, Denmark	
4. Scatternet Formation for Bluetooth Networks with Dynamic Membership	2028
Kenichi Mase, Takahiro Matsui, Tadachi Sato, Niigata University, Japan	
5. Wireless Bridging and Routing Method Employing a Novel Frame Transfer Protocol with Shortcut	2032
Takeo Ichikawa, Masataka Iizuka, Masahiro Morikura, Hideaki Matsue, NTT Corporation, Japan	

Poster Session 8: CDMA Systems

1. A New Slot Synchronization Scheme Robust to Timing Errors for W-CDMA	2038
--	-------------

Sang-yun Hwang, Jae-seok Kim, Yonsei University, Korea	
2. Optimum Downlink Antenna Weight Control Method for Adaptive Array Antennas in W-CDMA	2042
Manabu Mikami, Teruya Fujii, Japan Telecom Co., LTD., Japan	
3. Relaying in CDMA Networks: Pathloss Reduction and Transmit Power Savings	2047
Patrick Herhold, Wolfgang Rave, Gerhard Fettweis, Dresden University of Technology, Germany	
4. A Coloured Gaussian Model for CDMA Forward Link In-Cell Interference	2052
Geoffrey G. Messier, Nortel Networks, Canada;	
Witold A. Krzymien, University of Alberta, Canada	
5. Stretched Call Model for Next Generation Cellular Networks	2057
Sashidhar Lakkavalli, Suresh Singh, Portland State University, USA	
6. An Adaptive Thresholds Capacity Reservation Scheme for High Altitude Platform CDMA Systems	2062
Song Liu, Zhiheng Niu, Youshou Wu, Tsinghua University, China	
7. Sequence Adaptation for Cellular Systems	2066
Kin Kwong Leung, Tat Ming Lok, Chi Wan Sung, Chinese University of Hong Kong, Hong Kong	
8. Performance of Uplink Packet Services in WCDMA	2071
Konstantinos Dimou, Claudio Rosa, Troels B. Sorensen, Aalborg University, Denmark;	
Jeroen Wigard, Nokia Networks, Denmark;	
Preben E. Mogensen, Aalborg University, Denmark	
9. Adaptive Feedforward Amplifier Using Digital Controller	2076
Sanggee Kang, Unghee Park, Kyunghee Lee, ETRI, Korea;	
Seongyang Hong, Chnugnam National University, Korea	
10. A Cumulant-Based 2D-Rake Receiver for CDMA System over Frequency-Selective Fading Channels	2080
Wei Yang, Zhenhui Tan, Northern Jiaotong University, China	
11. Control Channel Design for High Speed Downlink Shared Channel for 3GPP W-CDMA, Rel-5	2085
Amitava Ghosh, Rapeepat Ratasuk, Colin Frank, Robert Love, Ken Stewart, Eoin Buckley, Motorola Inc., USA	
12. A Novel DS/SS System with Complex Chaotic Spreading Sequence	2090
Su Myat Htut, Ajeesh.P Kurian, Sadasivan Puthusserypady, National University of Singapore, Singapore	

Session 9A: Equalization/Channel Estimation 4

1. Low-Biased Doppler Frequency Estimation Scheme Employing Variable Prefilter and Sampling Rate	2095
Seok Ho Chang, Hee Jun Lee, LG Electronics Inc., Korea	
2. A Study on Channel Estimation Methods for MC-CDMA Systems	2101
Atsushi Nagate, Hiroyoshi Masui, Teruya Fujii, Japan Telecom Co. Ltd., Japan	
3. Double Decision-Directed Order Adaptive Weighted Moving Average Channel Estimator with Velocity Estimator for WCDMA Reverse Link Receiver	2106
Young-Yong Lee, Samsung Electronics Co., Ltd., Korea;	
Joo Hyun Do, Sungkyunkwan University, Korea;	
Sung-Hyun Chung, A-LOGICS Co., Ltd., Korea;	
Min-Joong Rim, Dongguk University, Korea;	
Jae-Min Ahn, Chungnam National Univerty, Korea;	
Hyung-Jin Choi, Sungkyunkwan University, Korea	
4. Channel Estimation for Downlink UMTS RAKE Receivers	2110
Lorenzo J. Tardon, Isabel Barbancho, Ana M. Barbancho, J. Tomas Entrambasaguas, ETSI de Telecomunicacion, Spain	
5. Performance of Channel Estimation Techniques for MC-CDMA Systems	2115
Yoshitaka Hara, Akinori Taira, Takashi Sekiguchi, Mitsubishi Electric Corporation, Japan	

Session 9B: Modulation and Coding 2 — Turbo Codes (1)

1. Packet Error Rate Analysis and its Reduction by Known Bits Insertion for Turbo Code in 100Mbps OFCDM System	2120
O. Kato, Panasonic Mobile Communications Co., Ltd., Japan;	
A. Matsumoto, Panasonic Mobile Communications Kanazawa R&D Lab. Co., Ltd., Japan;	
K. Fukawa, H. Suzuki, Tokyo Institute of Technology, Japan	
2. Turbo Equalization Using Non-Systematic and Recursive Systematic Convolutional Codes	2125
Vladimir D. Trajkovic, Predrag B. Rapajic, University of New South Wales, Australia	
3. Turbo Code with Power Reallocation	2130
Sang Wu Kim, Sung-Joon Park, Korea Advanced Institute of Science and Technology, Korea	
4. Bit-Level Stopping in Turbo Decoding	2134
Dong Ho Kim, Sang Wu Kim, Korea Advanced Institute of Science and Technology, Korea	
5. Dynamic Assignment of Probability Distributions of Extrinsic Information for Turbo Decoding over AWGN and Rayleigh Fading channels	2139

Session 9C: Interference Cancellation/MUD 3

1. Improving the Performance of ALOHA System Utilizing Coded Multi-User Detection	2144
Yunzhou Li, Shidong Zhou, Jing Wang, Tsinghua University, China	
2. Multi-User Detection in DS-CDMA Systems: a Conjugate-Gradient Implementation	2148
Ali Al Housseini, Thierry Chonavel, Samir Saoudi, Mahmoud Ammar, ENST-Bretagne, France	
3. Recursive Interference Canceller Using Slope Optimized Soft Limiter for DS-CDMA Downlink Channels in Frequency Selective Fading	2152
Bong-Hee Lee, Jae-Choon Jeon, Byung-kwan Jang, In-Kwan Hwang, Chungbuk National University, Korea	
4. Simple Iterative Chip-by-Chip Multiuser Detection for CDMA Systems	2157
Lihai Liu, W. K. Leung, Li Ping, City University of Hong Kong, Hong Kong	
5. On System Capacity and Coverage Improvements by Linear Multiuser Detection for UMTS	2162
Armin Dekorsy, Stefan Brueck, Lucent Technologies, Germany	

Volume 4

Session 9D: Adaptive Modulation and Coding (AMC) 2

1. Switching Threshold and Coding-Rate Optimisation for Turbo Convolutional and Turbo BCH Coded Adaptive Modulation	2167
T.H. Liew, Lajos Hanzo, University of Southampton, UK	
2. Impacts of Higher Order Modulation on HS-DSCH System Performance	2172
Eva Englund, Ke Wang Helmersson, Magnus Persson, Maria Samuelsson, Stefan Parkvall, Ericsson Research, Sweden	
3. Performance of Adaptive Multirate (AMR) Voice in GSM and WCDMA	2177
Harri Holma, Juan Melero, Janne Vainio, Timo Halonen, Jari Mäkinen, Nokia Networks, Finland	
4. SVD Pre/Post-Rake with Adaptive Trellis Coded Modulation	2182
Jin-Kyu Han, Dong-Ku Kim, Han-Kyu Park, Yonsei University, Korea	
5. Performance Analysis of the Adaptive Hybrid Search Code Acquisition Algorithm for Cellular CDMA Systems	2187
Hyung-Rae Park, Yeon-Sil Yang, Sang-Sik Yoon, Sang-Ho Lee, Hankuk Aviation University, Korea	

Session 9E: CDMA System 9

1. On the Use of QOF Functions with RC3 in Walsh Code Limited Base Station Deployments	2192
Levent Aydin, Walid Hamdy, Qualcomm Inc., USA	
2. On Optimizing SCH Burst Duration in CDMA2000	2196
Sunil Kandukuri, Walid Hamdy, Levent Aydin, Qualcomm Inc., USA	
3. A Two-Stage Adaptive MMSE Detector for Synchronous DS-CDMA System in a Rayleigh Fading Channel	2202
Hye Jeong Lee, Jae Hong Lee, Seoul National University, Korea	
4. A Highly Efficient Adaptive Digital Predistortion Amplifier for IMT-2000 Base Station	2206
Tokuro Kubo, Nobukazu Fudaba, Hiroyoshi Ishikawa, Hajime Hamada, Kazuo Nagatani, Hiroyuki Hayashi, Toru Maniwa, Yasuyuki Oishi, Fujitsu Laboratories LTD., Japan	
5. On the Validity of the Gaussian Approximation for Performance Analysis of TH-CDMA/OOK Impulse Radio Networks	2211
Khairi Ashour Hamdi, UMIST, UK; Xuanye Gu, BTexact Technologies, UK	

Session 9F: Power Control 1

1. Multi-Objective Totally Distributed Power and Rate Control for Wireless Communications	2216
Mohammed Elmusrati, Heikki Koivo, Helsinki University of Technology, Finland	
2. Subcarrier Allocation and Power Control for QoS Provision in the Presence of CCI for the Downlink of Cellular OFDMA Systems	2221
Slawomir Pietrzak, Radio Access Network Unit PTC, Poland; Gerard J.M. Janssen, Delft University of Technology, the Netherlands	
3. Pathloss-Aided Closed Loop Transmit Power Control for 3G UTRA TDD	2226

Sung-Hyuk Shin, Chang-Soo Koo, Donald Grieco, Ariela Zeira, InterDigital Communications Corp., U.S.A.	2231
4. A Robust Scheme for Cellular Power Control	
Ananth Subramanian, Nima Khajehnouri, Ali H. Sayed, University of Los Angeles, California, USA	
5. Downlink Channel Estimation and Power Control in CDMA Systems	2236
Hoon Kim, Jayong Koo, Keunyoung Kim, Youngnam Han, Information and Communications University, Korea	

Session 9G: Wireless Networks 3 — Mobile IP

1. A Study on Autonomous Neighbor Access Router Discovery for Mobile IP	2241
Natsuko Ono, Toru Kimura, Teruya Fujii, Japan Telecom Co., Ltd., Japan	
2. Transmission Quality Evaluation of Hierarchical Mobile IPv6 with Buffering Using Test Bed	2246
Hideaki Takahashi, Ryoichi Kobayashi, Ichiro Okajima, Narumi Umeda, NTT DoCoMo Inc., Japan	
3. QoS Support in IP/MPLS-Based Radio Access Networks	2251
Feng Li, Hoang M. Nguyen, Winston K.G. Seah, Institute for Infocomm Research, Singapore	
4. An Enhanced Mechanism for Supporting Mobile Networks in Mobile IP	2256
Chia-Ho Ou, Kuo-Feng Ssu, Hewijin Christine Jiau, National Cheng Kung University, Taiwan	
5. Integration of Micro-Mobility with QoS in IP/MPLS-Based Radio Access Networks	2261
Hoang Minh Nguyen, Feng Li, Qunying Xie, Institute for Infocomm Research, Singapore	

Session 9H: WLAN/Ad Hoc Network 9 — Topics in Multi-hop Wireless Networks (2)

1. Efficient Two-Hop Wireless Channel Access Protocol	2266
Hyunsun Kwak, Susumu Yoshida, Kyoto University, Japan	
2. On Connectivity and Mobility in Mobile Multi-Hop Wireless Networks	2271
Keisuke Nakano, Yuko Shirai, Masakazu Sengoku, Niigata University, Japan; Shoji Shinoda, Chuo University, Japan	
3. Performance Improvement of TCP on a Wireless Ad Hoc Network	2276
Masashi Sugano, Osaka Prefecture College of Health Sciences, Japan; Masayuki Murata, Osaka University, Japan	
4. Performance Evaluation of a Time Division Multi-Hop Relay Scheme in CDMA Cellular Networks	2281
Shinji Takeda, Atsushi Fujiwara, Hitoshi Yoshino, Toru Otsu, NTT DoCoMo Inc., Japan	
5. Hop Distances in Homogeneous Ad Hoc Networks	2286
Christian Bettstetter, Joerg Eberspaecher, Technische Universitat Munchen, Germany	

Poster Session 9: Satellite System & Modulation and Coding

1. Real-time Estimation of Rain Attenuation on the Satellite Link	2291
Joo-Hwan Lee, Yong-Seok Choi, , ETRI, Korea, Jung-Ki Pack, Chung-nam National University, Korea	
2. Effective Access Scheme of Reverse Link in IP Packet Based Satellite Access Network	2295
Taesoo Kwon, Korea Advanced Institute of Science and Technology, Korea; Kwangjae Lim, Electronics and Telecommunications Research Institute, Korea; Dong-Ho Cho, Korea Advanced Institute of Science and Technology, Korea	
3. Dynamic Location Update Strategy in LEO Systems	2300
Wang Liang, Zhang Nai-tong, Harbin Institute of Technology, China	
4. A Novel Tracking Control Realization of Phased Array Antenna for Mobile Satellite Communications	2305
Seong Ho Son, Soon Young Eom, Soon Ik Jeon, Electronics and Telecommunications Research Institute, Korea	
5. LDPC and Turbo Coding Assisted Space-Time Block Coded OFDM	2309
M.Y. Alias, F. Guo, S.X. Ng, T.H. Liew, Lajos Hanzo, Univ. of Southampton, UK	
6. Simulations of Communication Systems via Integrated Variance Reduction Techniques	2314
Adrian Bohdanowicz, Jos H. Weber, Delft University of Technology, Netherlands	
7. Multi-Rate Parity Accumulator Accumulator Codes	2319
Sung Ik Park, ETRI, Korea; Kyeongcheol Yang, POSTECH, Korea; Seung Won Kim, ETRI, Korea	
8. Sphere Decoding-Based Iterative MAP Receiver for Spatial Multiplexing Systems	2324
Seung Young Park, Samsung Advanced Institute of Technology, Korea; Soo Ki Choi, Chung Gu Kang, Korea University, Korea; Ki Ho Kim, Samsung Advanced Institute of Technology, Korea	
9. Analysis of Convolutional Code Performance in Generalized Fading Channels	2329

Oliver Klein, Ingolf Held, Ericsson Eurolab, Germany	
10. Performance of 8SQAM in a Nonlinearly Amplified Multichannel Interference Environment	2334
Bong-hoon Seoung, Jong-soo Seo, Yonsei University, Korea	
11. Saving Memory in Turbo Trellis Coded Modulation Using the Sliding Window	2339
Nam kyung Kim, Myong Seop Yang, Chonbuk National University, Korea;	
Soon Young Kim, KT, Korea;	
Moon ho Lee, Chonbuk National University, Korea	

Session 10A: Equalization/Channel Estimation 5

1. A Novel Channel Estimation Method for OFDM Transmission Technique under Fast Time-Variant Fading Channel	2343
Tadayuki Fukuhara, Hao Yuan, Yoshio Takeuchi, KDDI R&D Laboratories Inc., Japan;	
Hideo Kobayashi, Mie University, Japan	
2. Joint ML Estimation of I/Q Mismatch, DC Offset, Carrier Frequency, and Channel for Direct-Conversion Receivers	2348
Gate Gil, Il-Hyun Sohn, Korea Advanced Institute of Science and Technology, Korea;	
Young Ik Song, Samsung Thales Co., Ltd, Korea;	
Jin Kyu Park, Agency for Defense Development, Korea;	
Yong H.Lee, Korea Advanced Institute of Science and Technology, Korea;	
3. A Generalization of Multiple-Symbol Differential Detection and its Application to Fast Time-Varying Fading Channels	2353
Hiroshi Kubo, Kazuo Tanada, Akihiro Okazaki, Keishi Murakami, Mitsubishi Electric Corp., Japan	
4. Decision-Directed Channel Estimation Method for OFDM Systems with High Velocities	2358
Jianjun Ran, Rainer Grunheid, Hermann Rohling, Technical University of Hamburg-Harburg, Germany;	
Edgar Bolinth, Ralf Kern, Siemens AG, Germany	
5. Hybrid Stable Fast Kalman and Variable Step-Size LMS Decision Feedback Equalizer for 8-VSB DTV	2362
Jong-Seob Baek, Young-Jin Lee, Yong-Tae Lee, Jong-Soo Seo, Yonsei University, Korea	

Session 10B: Modulation and Coding 3 — Turbo Codes (2)

1. Radial Basis Function Assisted Reduced Complexity In-Phase/Quadrature-Phase Turbo Equalisation of Coded Modulation Schemes	2367
M.S. Yee, S.X. Ng, Lajos Hanzo, University of Southampton, UK	
2. Parallel Decoding of Turbo Product Codes for High Data Rate Communication	2372
Xiujun Zhang, Ming Zhao, Shidong Zhou, Jing Wang, Tsinghua University, China	
3. Low Complexity Stopping Criteria for UMTS Turbo-Decoders	2376
Frank Gilbert, Frank Kienle, Norbert When, University of Kaiserslautern, Germany	
4. Quasi-Complementary Turbo Codes (QCTC) for Applications in High-Data-Rate Systems	2381
Min Goo Kim, Sang Hyuk Ha, Samsung Electronics, Korea	
5. Optimized Parameter Design of Linear Dispersion Codes in MIMO Channels	2386
Xiaojian Lu, Lin Dai, Ming Zhao, Jing Wang, Tsinghua University, China	

Session 10C: Interference Cancellation/MUD 4

1. Log-Likelihood Ratio Based Successive Interference Cancellation in CDMA Systems	2390
Sang Wu Kim, Young-Jun Hong, Korea Advanced Institute of Science and Technology, Korea	
2. Minimum Joint Probability of Error Based Adaptive Multiuser Detection for Multipath DS-CDMA Channels	2394
Aditya Dua, U.B. Desai, Ranjan K. Mallik, Indian Institute of Technology, India	
3. Neural Networks for Multi-User Detection in MC-CDMA Systems	2399
Florent Carlier, Fabienne Nouvel, IETR, France	
4. Semi-Blind Multiuser Detector Based on Auxiliary-Vector	2404
Bin Xu, Chenyang Yang, Shiyi Mao, Beijing University of Aeronautics and Astronautics, China	
5. Code-Constrained Blind Multiuser Detection of Asynchronous CDMA Signals in Multipath Channels with CMA Equalization	2408
Yonwoo Yoon, Hyung-Myung Kim, Korea Advanced Institute of Science and Technology, Korea	

Session 10D: Diversity 1

1. Capacity Gain from Transmit Diversity Methods in Limited Bandwidth GSM/EDGE Networks	2413
Jari Hulkonen, Timo Kähkönen, Jyri Hämäläinen, Tero Korpi, Mikko Säily, Nokia Networks, Finland	
2. On the Performance of GSM/EDGE Transmit Diversity Schemes when Employing Dual-Polarized Antennas	2418
Jyri Hämäläinen, Risto Wichman, Helsinki University of Technology, Finland;	
Jari Hulkonen, Timo Kahkonen, Tero Korpi, Mikko Säily, Nokia Networks, Finland	
3. Interaction of Transmit Diversity and Proportional Fair Scheduling	2423
Lars T. Berger, Aalborg University, Denmark;	
Troels E. Kolding, Nokia Networks, Aalborg R&D, Denmark;	
Juan Ramiro-Moreno, Pablo Ameigeiras, Laurent Schumacher, Aalborg University, Denmark;	
Preben E. Mogensen, Aalborg University and Nokia Networks, Aalborg R&D, Denmark	
4. Performance Enhancement of Transmit Diversity Schemes Using Subarray Transmit Eigen-beamformer	2428
Hong-Cheol Kim, Yoan Shin, Won-Cheol Lee, Soongsil University, Korea	
5. A Hybrid Transmit Diversity Scheme of Prefilter and Transmit Adaptive Array in MISO Wireless CDMA Systems	2433
Sanhae Kim, Woncheol Lee, Yoan Shin, Soongsil University, Korea	

Session 10E: Transportation

1. Seamless Mobility Support for Mobile Networks on Vehicles across Heterogeneous Wireless Access Networks	2437
Eun Kyoung Paik, Yanghee Choi, Seoul National University, Korea	
2. SOTIS – A Self-Organizing Traffic Information System	2442
Lars Wischhof, André Ebner, Hermann Rohling, Technical University of Hamburg-Harburg, Germany;	
Matthias Lott, Rudiger Halfmann, Siemens AG, Germany	
3. Intelligent Controller Design for Electric Vehicle	2447
S. Poorani, K. UdayaKumar, S. Ranganarayanan, Anna University, India	
4. Design and Analysis of Highway Safety Communication Protocol in 5.9 GHz Dedicated Short Range Communication Spectrum	2451
Qing Xu, Raja Sengupta, University of California, USA;	
Daniel Jiang, DaimlerChrysler, Canada	
5. A Multicast Protocol in Ad hoc Networks Inter-Vehicles Geocast	2456
Abdelmalik Bachir, Abderrahim Benslimane, University of Avignon, France	

Session 10F: Power Control 2

1. Optimal Power Allocation for Relayed Transmissions over Rayleigh Fading Channels	2461
Mazen O. Hasna, Mohamed-Slim Alouini, University of Minnesota, USA	
2. Joint Power Allocation and Base-Station Assignment Based on Pricing for the Downlink in Multi-Class CDMA Networks	2466
Jang Won Lee, Ravi R. Mazumdar, Ness B. Shroff, Purdue University, USA	
3. Performance of CDMA Forward Channels with Random Puncturing	2471
Hichan Moon, Donald C. Cox, Stanford University, USA	
4. Quasi-Optimum Downlink Power Control of High Altitude Platform W-CDMA System	2476
Bazil Taha Ahmed, Miguel Calvo Ramon, Leandro Haro Ariet, UPM ETSI de Telecom., Spain	
5. Improving UTRA TDD Downlink Power Control with Asymmetrical Steps	2480
Janne Kurjeniemi, University of Jyvaskyla, Finland;	
Otto Lehtinen, Nokia Research Center, USA;	
Tapani Ristaniemi, University of Jyvaskyla, Finland	

Session 10G: Wireless Networks 4

1. Power and Frequency Efficient Virtual Cellular Network	2485
Eisuke Kudoh, Fumiuki Adachi, Tohoku University, Japan	
2. Enhanced Frequency Hopping for Deployments with Limited Spectrum	2490
Krishna Balachandran, Joseph H. Kang, Lucent Technologies, Bell Laboratories, USA	
3. An Adaptive Fault Tolerance Algorithm for Multimedia Cellular Networks	2495
Sungwook Kim, Pramod K. Varshney, Syracuse University, USA	
4. Multilayer Mobility Management for All-IP Networks: Pure SIP vs. Hybrid SIP/Mobile IP	2500
Christos Politis, Kar Ann Chew, Rahim Tafazolli, University of Surrey, UK	

5. Buffer Management for the Interactive Bearer in GERAN	2505
Hannes Ekström, Andreas Schieder, Ericsson Research, Germany	

Session 10H: WLAN/Ad Hoc Network 10 — Performances

1. Spectral Shape of UWB Signals – Influence of Modulation Format, Multiple Access Scheme and Pulse Shape	2510
Yves-Paul Nakache, Mitsubishi Electric Research Labs, USA;	
Andreas F. Molisch, Lund University, Sweden	
2. Receiver-Initiated Multiple Access Protocols for Spread Spectrum Mobile Ad Hoc Networks	2515
Yi-Sheng Su, Szu-Lin Su, Jung-Shian Li, National Cheng Kung University, Taiwan	
3. Performance Evaluation of Bluetooth Using Interference-Detection-Based Frequency Hopping	2520
SeungBeom Lee, Sin-Chong Park, Information and Communications University, Korea	
4. Performance Evaluation of CSMA/CA with Multiple-Variable Contention Window	2523
Wookwon Lee, Mohammad A. Khan, University of Arkansas, USA	
5. Adaptive Polling MAC Schemes for IEEE 802.11 Wireless LANs	2528
Young-Jae Kim, Young-joo Suh, Pohang University of Science & Technology, Korea	

Poster Session 10: Equalization/Channel Estimation & Diversity

1. A Joint Detection-Decoding Receiver with Reduced Complexity	2533
Hyungkeun Lee, Pramod K. Varshney, Syracuse University, USA	
2. Effect of Noise Variance in the Channel Estimation on Dual-MRC over Rayleigh Fading Channels	2538
Young-Chai Ko, Tao Luo, Gibong Jeong, Texas Instruments, USA	
3. Joint Weighted Least Squares Estimation of Frequency and Timing Offset for OFDM Systems over Fading Channels	2543
Pei-Yun Tsai, Hsin-Yu Kang, Tzi-Dar Chiueh, National Taiwan University, Taiwan	
4. A Multipath Fading Channel Model Applied to Fast UMTS Link Simulation with Channel Estimation	2548
Pierre Gelpi, Ahmed Saadani, Stefan Wendt, France Telecom R&D, France	
5. On Decoding and Equalization of Multidimensional Trellis-Coded OFDM Systems	2551
Pei-Chun Liu, Kwang-Cheng Chen, National Taiwan University, Taiwan	
6. Optimal Interpolators for Flexible Digital Receivers	2556
Nguyen Doan Vo, Tho Le-Ngoc, McGill University, Canada	
7. Optimised MLSE Equaliser for Fast Channel Tracking and Reliable Decoding When Using Space Time DPSK Block Codes for Future WPAN	2560
R. Cepeda, D. Gargin, M. Fitton, C. Leong, Toshiba Research Europe Limited, UK	
8. Particle Filtering for Joint Data-Channel Estimation in Fast Fading Channels	2565
Tanya Bertozzi, Didier Le Ruyet, CNAM, France;	
Gilles Rigal, DIGINEXT, France;	
Han Vu-Thien, CNAM, France	
9. Performance Study of Least-Squares Channel Estimation Based on Hard Decisions	2570
Samson Lasaulce, France Telecom R&D, France;	
Noura Sellami, ENSEA Laboratoire ETIS, France;	
Yi Yuan, Ahmed Saadani, France Telecom R&D, France	
10. Blind Joint Channel Estimation and Signal Decoding for Systems with Time-Varying Rayleigh-Fading Channels	2575
Ching-Shyang Maa, Chin-Tseng Huang, Yeong-Cheng Wang, Jiunn-Tsair Chen, National Tsing Hua University, Taiwan	
11. Performance Analysis of Equal Gain Combining 2D-RAKE Receiver in NAKAGAMI-Fading Channels	2579
Kaizhi Huang, Jing Wang, Youzheng Wang, Tsinghua University, China	
12. On Transmit Diversity for TD-SCDMA	2584
Ingolf Held, Almansor Kerroum, Synopsys, Germany	
13. LDPC-Based Space-Time Transmit Diversity Schemes with Multiple Transmit Antennas	2589
Hisashi Futaki, Tomoaki Ohtsuki, Tokyo University of Science, Japan	
14. A Simple Transmit Antenna Diversity Technique for OFDM and its Detection Using Viterbi Algorithm	2594
Jinho Choi, The University of New South Wales, Australia	

Session 11A: Equalization/Channel Estimation 6

1. PN Code Tracking for STBC Transmit Diversity RAKE Receivers in Closely Spaced Multipath Environments	2599
Bagawan S. Nugroho, Raja D. Balakrishnan, Hyuck M. Kwon, Wichita State University, USA;	
Dong H. Kang, Samsung Electronics, Korea	

2. Iterative Receiver Design in Rayleigh Fading Using Factor Graph	2604
Manyuan Shen, Huaning Niu, Hui Liu, University of Washington, USA	
3. Fast Symbol Timing Recovery Techniques for Burst-Mode Digital Demodulators	2609
Nguyen Doan Vo, Tho Le-Ngoc, McGill University, Canada	
4. Computationally Efficient Channel Estimation for Space-Time Block Coded System	2614
J.G. Sheng, A. Nallanathan, National University of Singapore, Singapore;	
T.T. Tjhung, Institute for Infocomm Research, Singapore	
5. MMSE Receiver Filter for CDMA1xEV-DV	2618
Seo Weon Heo, Jóng Han Lim, Seong Woo Ahn, Samsung Electronics, Korea	

Session 11B: Modulation and Coding 4 --- Modulation

1. Constrained Envelope Continuous Phase Modulation	2623
Tommy Svensson, Arne Svensson, Chalmers University of Technology, Sweden	
2. Performance Analysis for M-ary Orthogonal FSK with Hybrid Selection/Equal-Gain Combining over Nakagami Fading Channels	2628
Jay Cheng, Toby Berger, Cornell University, USA	
3. Hierarchical Modulation for Multimedia and Multicast Transmission over Fading Channels	2633
Md. Jahangir Hossain, University of Victoria, Canada;	
Pavan K. Vitthaladevuni, Mohamed-Slim Alouini, University of Minnesota, USA;	
Vijay K. Bhargava, University of Victoria, Canada	
4. Proposal of Channel Synthesized Modulation for Secured Access on Physical Layer	2638
Masayuki Orihashi, Yutaka Murakami, Youichi Nakagawa, Takashi Matsuoka, Matsushita Electric Industrial Co. Ltd., Japan	
5. DS-CDMA Receiver with Sigma-Delta Modulation Encoding	2644
Kaibin Huang, Po Shin Chin, Institute for Communications Research, Singapore;	
Kwee Tong Heng, Singapore Telecommunication Limited, Singapore	

Session 11C: Interference Cancellation/MUD 5

1. Matched Filter for Transmission over Channels with ISI Employing the Distribution of Interference	2648
Jurgen F. Roessler, Johannes B. Huber, University Erlangen-Nuremberg, Germany	
2. Capacity and Performance Gains through Temporal and Spatial Oversampling	2653
Ozge H. Koymen, Teresa H. Meng, Stanford University, USA	
3. An Adaptive ICI Self Cancellation Scheme to Compensate the Frequency Offset for OFDM System	2658
Yang Hongwei, Li Guangjie, Cai Liyu, Gui Luoning, Alcatel Shanghai Bell Co. Ltd., China	
4. Critical Load of Oversaturated Systems with Multistage Successive Interference Cancellation	2663
Frederik Vanhaverbeke, M. Moeneclaey, Ghent University, Belgium	
5. Effect of Antenna Element Separation on Performance of MAI Canceller Combined with Adaptive Array Antenna for DS-CDMA Systems	2667
Kazuto Yano, Shoichi Hirose, Susumu Yoshida, Kyoto University, Japan	

Session 11D: Diversity 2

1. Performance Analysis of Diversity Combining Method for OFDM Blind Carrier Synchronization	2672
Patrick J. Honan, Rajesh Ambati, Ufuk Tureli, Stevens Institute of Technology, USA	
2. Doppler Diversity for OFDM Wireless Mobile Communications: Part I: Frequency Domain Approach	2677
Byung-Chul Kim, Samsung Electronics Co. Ltd., Korea;	
I-Tai Lu, Polytechnic University, USA	
3. Doppler Diversity for OFDM Wireless Mobile Communications: Part II: Time-Frequency Processing	2682
Byung-Chul Kim, Samsung Electronics Co. Ltd., Korea;	
I-Tai Lu, Polytechnic University, USA	
4. Throughput Analysis of Three Multiuser Diversity Schemes	2686
Fredrik Florén, Ove Edfors, Lund University, Sweden;	
Bengt-Arne Molin, Axis Communications AB, Sweden	
5. A Rake Finger Grid for Asynchronous DS-CDMA Systems Using LMMSE Tap Weight Estimation	2691
Volker Simon, Lars Schmitt, ISS, RWTH-Aachen, Germany;	
Thomas Grundler, Christoph Schreyogg, Siemens AG, Germany;	
Heinrich Meyr, ISS, RWTH-Aachen, Germany	

Session 11E: Location Management

1. Database Correlation Method for UMTS Location	2696
Suvi Ahonen, Heikki Laitinen, VTT Information Technology, Finland	
2. Kalman-Filter-Based Predictive Location Management for PCS Networks	2701
Kenneth W. Shum, Chi Wan Sung, City University of Hong Kong, Hong Kong	
3. Detection of a Line-of-Sight Connection to a UMTS Base Station for Increased Location Accuracy of User Terminals	2706
Thomas Hesse, University of Paderborn, Germany	
4. CDMA Location Using Multiple Antennas and Interference Cancellation	2711
Alireza Tarighat, Nima Khajehnouri, Ali H. Sayed, University of California, USA	
5. Mobile Station Location Using Hybrid GPS and a Wireless Network	2716
Hyung Chul Son, Jang Gyu Lee, Seoul National University, Korea; Gyu In Jee, Konkuk University, Korea	

Session 11F: HARQ

1. Investigation of Hybrid ARQ Performance for TDD CDMA HSDPA	2721
Jinwen Zhang, Weifeng Cao, Mugen Peng, Wenbo Wang, Beijing University of Posts and Telecommunications, China	
2. Rate Compatible Punctured Turbo-Coded Hybrid ARQ for OFDM in a Frequency Selective Fading Channel	2725
Deepshikha Garg, Fumiaki Adachi, Tohoku University, Japan	
3. Throughput of RCPT Hybrid ARQ for DS-CDMA with Diversity Reception and Rake Combining	2730
Deepshikha Garg, Fumiaki Adachi, Tohoku University, Japan	
4. Performance Evaluation of some Hybrid ARQ Schemes in IEEE 802.11a Networks	2735
Emilio Calvanese Strinati, Sebastien Simoens, Motorola Labs Paris, France; Joseph Boutros, ENST, France	
5. Performance Analysis of Type III HARQ with Turbo Codes	2740
Wang Yafeng, Zhang Lei, Yang Dacheng, Beijing University of Posts and Telecommunications, China	

Session 11G: Wireless Networks 5

1. Mobility and Traffic Parameters for Simulating Interoperating UMTS and HIPERLAN/2 MTMR Enabled Networks	2745
Dimitrios I. Axiotis, Fotios I. Lazarakis, National Technical University of Athens, Greece; C. Vlahodimitropoulos, COSMOTE, Greece	
2. WLANs with Extended Communication Ranges	2750
Mischa Dohler, Hamid Aghvami, King's College London, UK	
3. A Case Study of Policy-based QoS Management in 3G Networks	2755
Mi Kyoung Kim, Kiho Nam, Jaeki Lee, Hwang-Soo Lee, KAIST, Korea	
4. An Accurate Heuristic Approach for UMTS RLC Delay Statistics Evaluation	2760
Michele Rossi, Michele Zorzi, University of Ferrara, Italy	
5. Effect of Signaling Network Topology in Cellular System Performance	2765
J. Roberto B. de Marca, Rodigo C.D. de Carvalho, Cetuc - PUC/Rio, Brazil	

Session 11H: WLAN/Ad Hoc Network 11

1. Exploring the Energy-Latency Tradeoff of Geographic Random Forwarding for Ad Hoc and Sensor Networks	2770
Michele Zorzi, Universita di Ferrara, Italy; Ramesh R. Rao, University of California at San Diego, USA	
2. Enhancement of IEEE 802.11 Distributed Coordination Function with Exponential Increase Exponential Decrease Backoff Algorithm	2775
Nah-Oak Song, Byung-Jae Kwak, Jabin Song, Leonard E. Miller, National Institute of Standards and Technology, USA	
3. A Modified HMRSVP Scheme	2779
Ye Min-hua, Zhang Ying, Zhang Hui-min, Liu Yu, Beijing Univ. of Posts and Telecommunications, China	
4. Efficient Procedure for Avoiding Redundant Data Retransmissions in IEEE 802.11 WLAN	2783
Hiroyuki Yomo, Ramjee Prasad, Aalborg University, Denmark	
5. A Software and Hardware Evaluation of Revolutionary Turbo MIMO OFDM Schemes for 5GHz WLANs	2788
T. Horseman, J. Webber, M.K. Abdul-Aziz, R. Piechocki, M. Beach, A. Nix, P. Fletcher, University of Bristol, UK	

Poster Session 11: Interference Cancellation/MUD & Transceiver Architecture

1. Finite Field Wavelet Spread Signature CDMA with Hybrid Successive and Intracode Interference Cancellation	2793
Jiann-Horng Chen, St. John's & St. Mary's Institute of Technology, Taiwan;	
Kuen-Tsair Lay, National Taiwan University of Science and Technology, Taiwan	
2. On the Performance of Multi-Stage Multi-User Detection Assisted Fast-FH/MFSK	2798
Kiyoshi Hamaguchi, Communications Research Laboratory, Japan;	
Lie-Liang Yang, Lajos Hanzo, University of Southampton, UK	
3. Pre-Rejection of Distorted Speech for Speech Recognition in Wireless Communication Channel	2803
Joon-Hyuk Chang, Dong Jin Seo, Young-Joon Kim, Nam Soo Kim, Seoul National University, Korea	
4. Performance Analysis of a Multistage MPIC in 16-QAM CDMA Systems over Multipath Rayleigh Fading Channels	2807
KyunByoung Ko, Yonsei University, Korea;	
Dongseung Kwon, Daesoon Cho, ETRI, Korea;	
Changeon Kang, Daesik Hong Yonsei University, Korea	
5. Adaptive Minimum Symbol-Error-Rate CDMA Linear Multiuser Detector for Pulse-Amplitude Modulation	2812
A.K. Samingan, S. Chen, Lajos. Hanzo, University of Southampton, U.K	
6. Robust Multiuser Detection Based on Minimax M-Beamforming for Mobile Communications	2817
Vladimir Katkovnik, Moon-Sik Lee, Yong-Hoon Kim, Kwangju Institute of Science and Technology, Korea	
7. Iterative Multiuser Acquisition for DS-CDMA Systems	2822
Tsung-Cheng Wu, I-Shou University, Taiwan	
8. Multipath Interference Reduction Property by Using Multipath Interference Correlative Timing Throughout for DS-CDMA Systems	2827
Tsuyoshi Hasegawa, Masahiko Shimizu, Fujitsu Laboratories Ltd., Japan	
9. A Study of Orthogonal Matched Filters for Interference Cancellation in the Situation that Different Spreading Codes Exist	2832
Keigo Takada, Katsuya Mizutani, Kenta Umebayashi, Yokohama National University, Japan;	
Yoshihiro Hase, Shingo Ohmori, Fujinobu Takahashi, Independent Administrative Institution, Japan;	
Ryuji Kohno, Yokohama National University, Japan	
10. A State-Machine Based Design of Adaptive Wireless MAC Layer	2837
Z. Xiao, T.S. Randhawa, New Media Innovation Center, Canada;	
R.H.S. Hardy, Simon Fraser University, Canada	
11. Implementation of Reconfigurable Transceiver based on Digital IF for Multiple Wideband CDMA Signals	2842
Jae Ho Jung, Kwang Chun Lee, Deuk Soo Lyu, ETRI, Korea	
Quality-based Auto-tuning of Cell Uplink Load Level Targets in WCDMA	2847
Albert Höglunda, Janne Pöllönena, Kimmo Valkealahti, Nokia Research Center, Finland	
Jaana Laiho, Nokia Networks, Finland	
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